



# Two-Phase Continuum Models for Geophysical Particle-Fluid Flows

Seminar: 21 March - 15 April 2016

**Sediment gravity flows in Quesnel Lake  
caused by the catastrophic Mount  
Polley mine tailings dam failure**

Ray Kostaschuk

Simon Fraser University

# Outline

- The Tailings Dam Failure and Subaerial Debris Flows in Hazeltine Creek
- Subaqueous Gravity Flows in Quesnel Lake
- Erosion by Subaqueous Debris Flows in Quesnel Lake
  - Preliminary Results From the Iverson (2012) Entrainment Model
- Geoflo19: Modelling Debris Flow Deposition in Quesnel Lake

Date	Location	Parent company	Ore type	Type of incident	Release	Impacts
2015, Nov. 21	Hpakant, Kachin state, Myanmar	†	jade	waste heap failure	†	at least 113 people killed
2015, Nov. 5	Germão mine, Bento Rodrigues, distrito de Mariana, Região Central, Minas Gerais, Brazil	<a href="#">Samarco Mineração S.A.</a> (50% <a href="#">IHIP Billiton</a> , 50% <a href="#">Vale</a> (→))	iron	failure of two tailings dams holding a combined 62 million m <sup>3</sup> (apparently, the Fundão dam broke first, releasing tailings into the Santarém dam, which failed then as well)	32 million m <sup>3</sup> <a href="#">Video of the flow slide</a> (→)	slurry wave flooded town of Bento Rodrigues, destroying 158 homes, at least 17 persons killed and 2 reported missing; slurry pollutes North Gualano River, Carmel River and Rio Doce over 663 km, destroying 15 square kilometers of land along the rivers and cutting residents off from potable water supply
2014, Sep. 10	Herculano mine, Itabirito, Região Central, Minas Gerais, Brazil	<a href="#">Herculano Mineração Ltda.</a> (→)	iron	tailings dam failure	†	two workers killed and one missing
2014, Aug. 7	Buenavista del Cobre mine, Cananea, Sonora, Mexico	<a href="#">Southern Copper Corp.</a> (→) ( <a href="#">Grupo México</a> (→))	copper	tailings dam failure	40,000 m <sup>3</sup> of copper sulphate	flow into the 420km-long Bacanuchi river waterway, a tributary of the Sonora River, directly affecting 800,000 people
2014, Aug. 4	Mount Polley mine, near Likely, British Columbia, Canada	<a href="#">Imperial Metals Corp.</a> (→)	copper, gold	tailings dam failure due to foundation failure ( <a href="#">video details</a> )	7.3 million m <sup>3</sup> of tailings, 10.6 million m <sup>3</sup> of water, and 6.5 million m <sup>3</sup> of interstitial water	tailings flowing into adjacent Polley Lake and, through Haseltine Creek, into Quessell Lake (Mitchell Bay)

# British Columbia



500 km

Vancouver





Mt Polley  
Mine

West Arm

Quesnel Lake

20 km

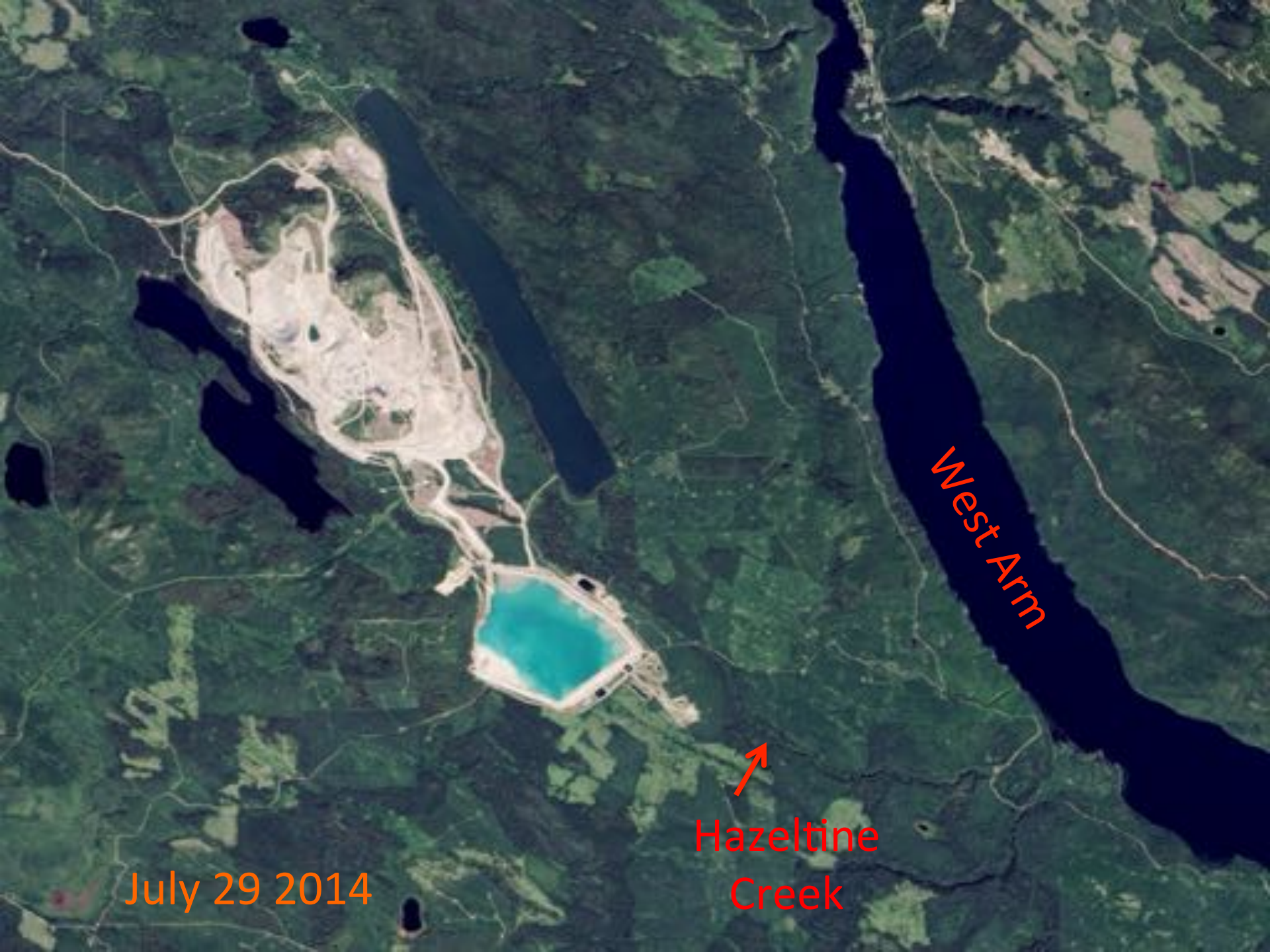


# The Tailings Dam Failure and Subaerial Debris Flows in Hazeltine Creek

- Early on August 4, 2014, a tailings dam failure occurred at the Mount Polley Mine causing water and toxic tailings to be released to Polley Lake, Hazeltine Creek and Quesnel Lake
- The failure of the dam was caused by a combination of poor design, poor maintenance, and inadequate inspection by the British Columbia government

<https://www.youtube.com/watch?v=VYYwzAvQIF8>



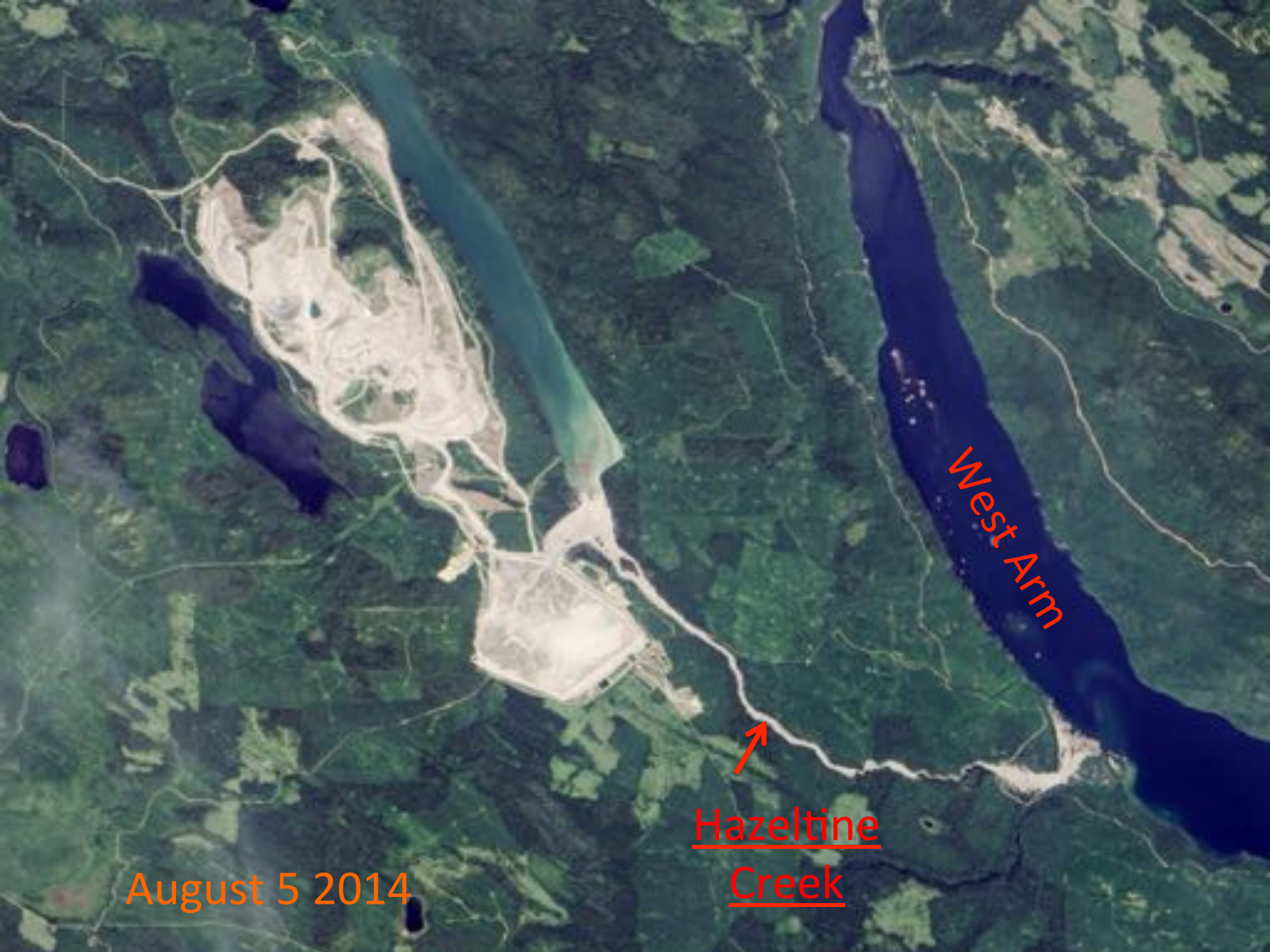


West Arm

Hazeltine  
Creek

July 29 2014





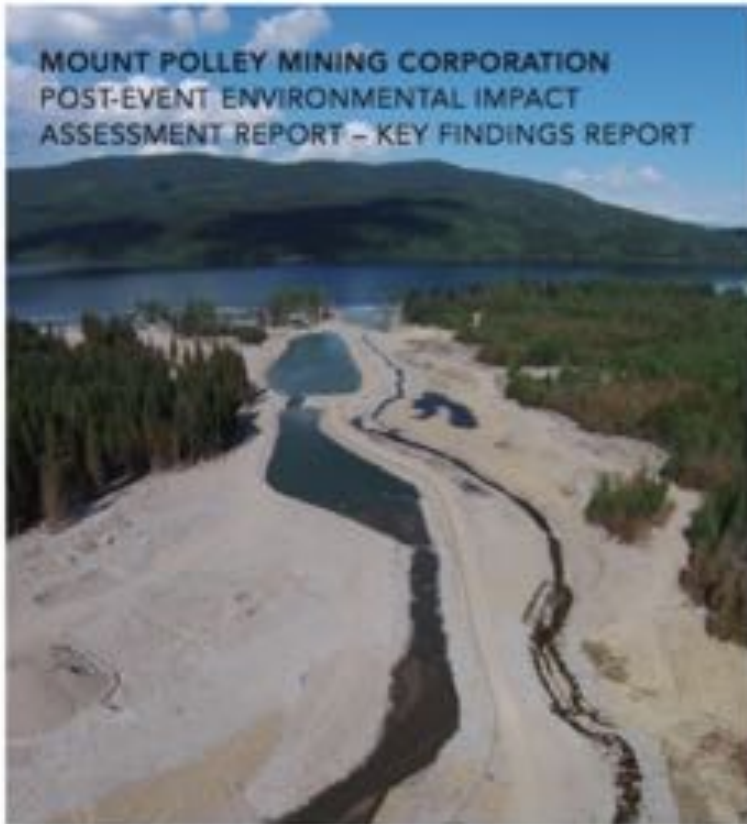
West Arm



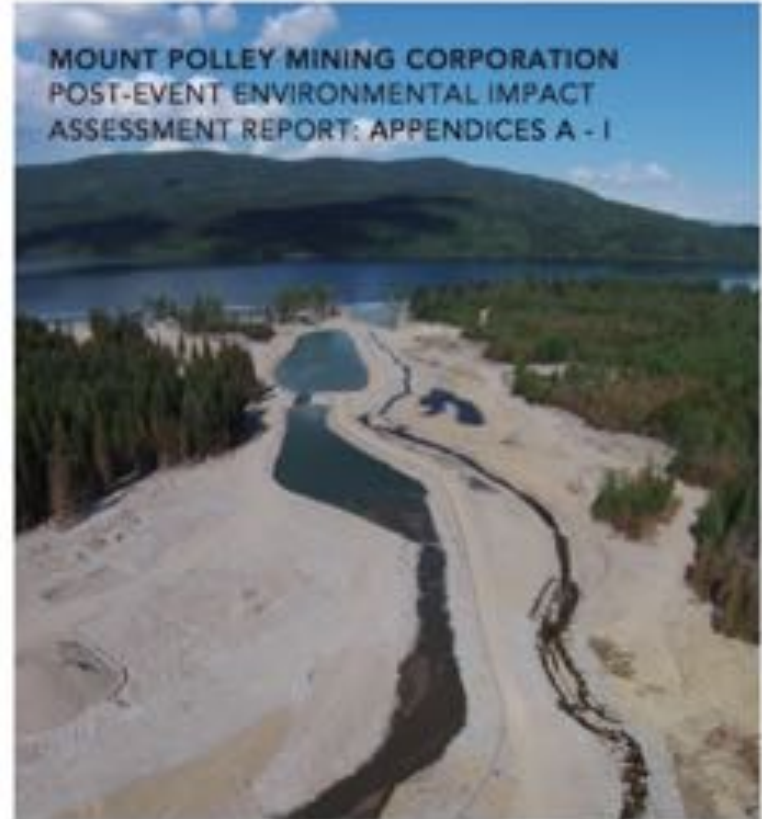
Hazeltine  
Creek

August 5 2014

JUNE 5, 2015



Mount Polley Mining Corporation  
an Imperial Metals company



Mount Polley Mining Corporation  
an Imperial Metals company













<https://www.youtube.com/watch?v=xAltFxc8bME>

grey layer of  
fine material

red layer of  
sandy material

topsoil

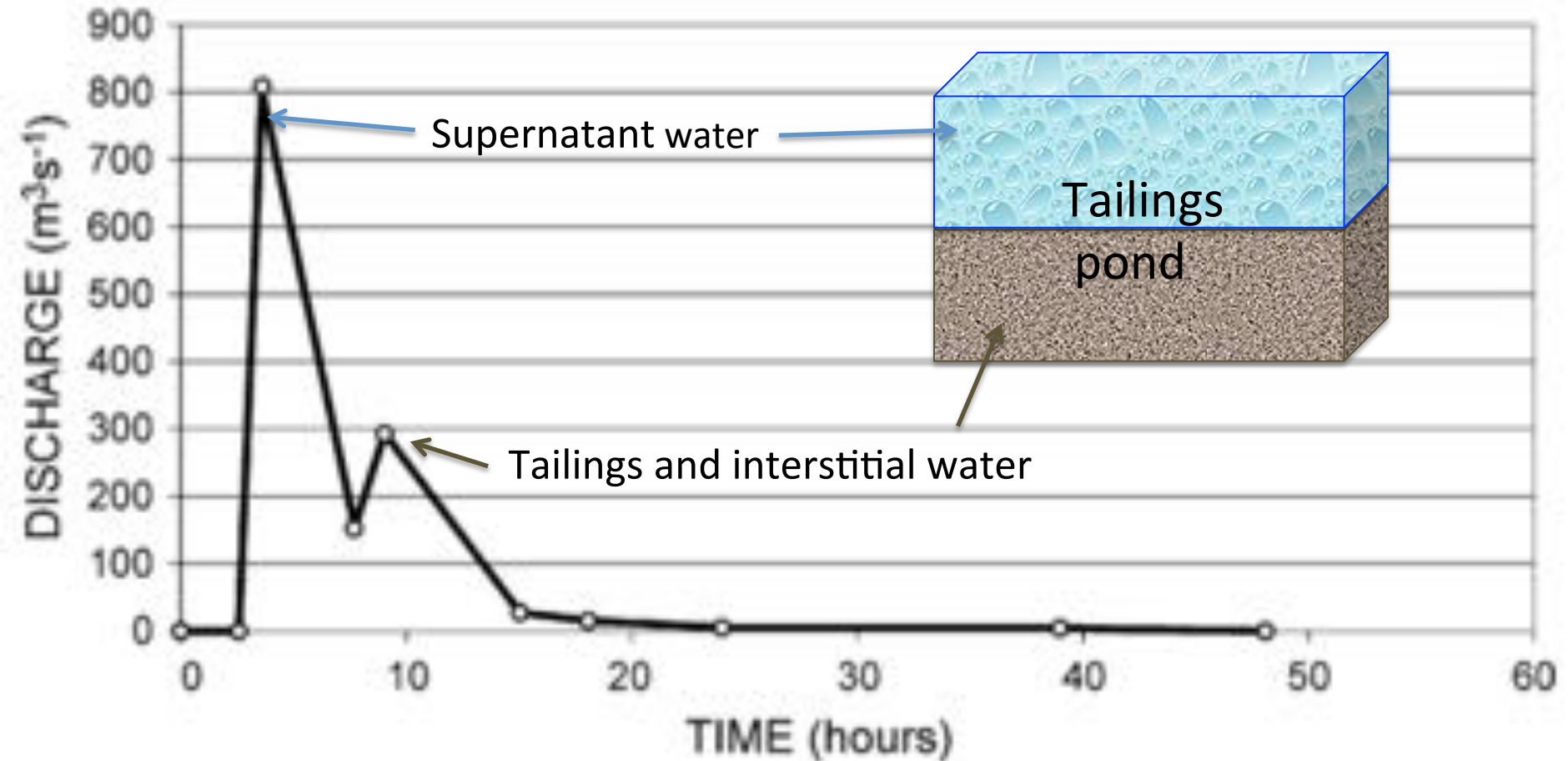




## Volume estimates for tailings dam failure

Volume Estimation	Total
Supernatant water (Mm <sup>3</sup> )	10.6
Tailings solids (Mm <sup>3</sup> )	7.3
Interstitial water (Mm <sup>3</sup> )	6.5
Construction materials (Mm <sup>3</sup> )	0.6
Total outflow volume (Mm <sup>3</sup> )	25.0
Net volume of eroded material (Mm <sup>3</sup> )	0.6 To 1.7
Total volume of the event (Mm <sup>3</sup> ) <sup>1</sup>	25.6 To 26.7

# TAILINGS FLOOD HYDROGRAPH IN THE EL GUIJO GAUGE STATION





**low-energy  
debris flow**

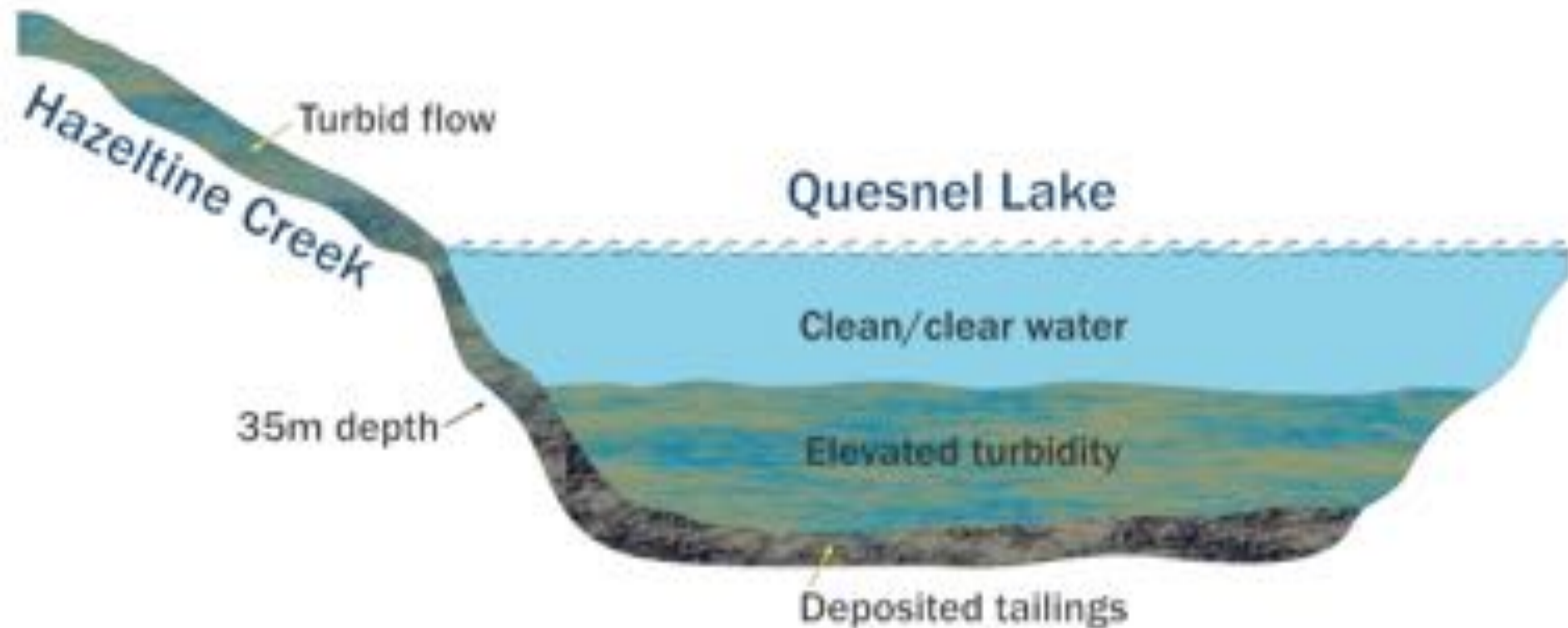
**high-energy  
debris flow**



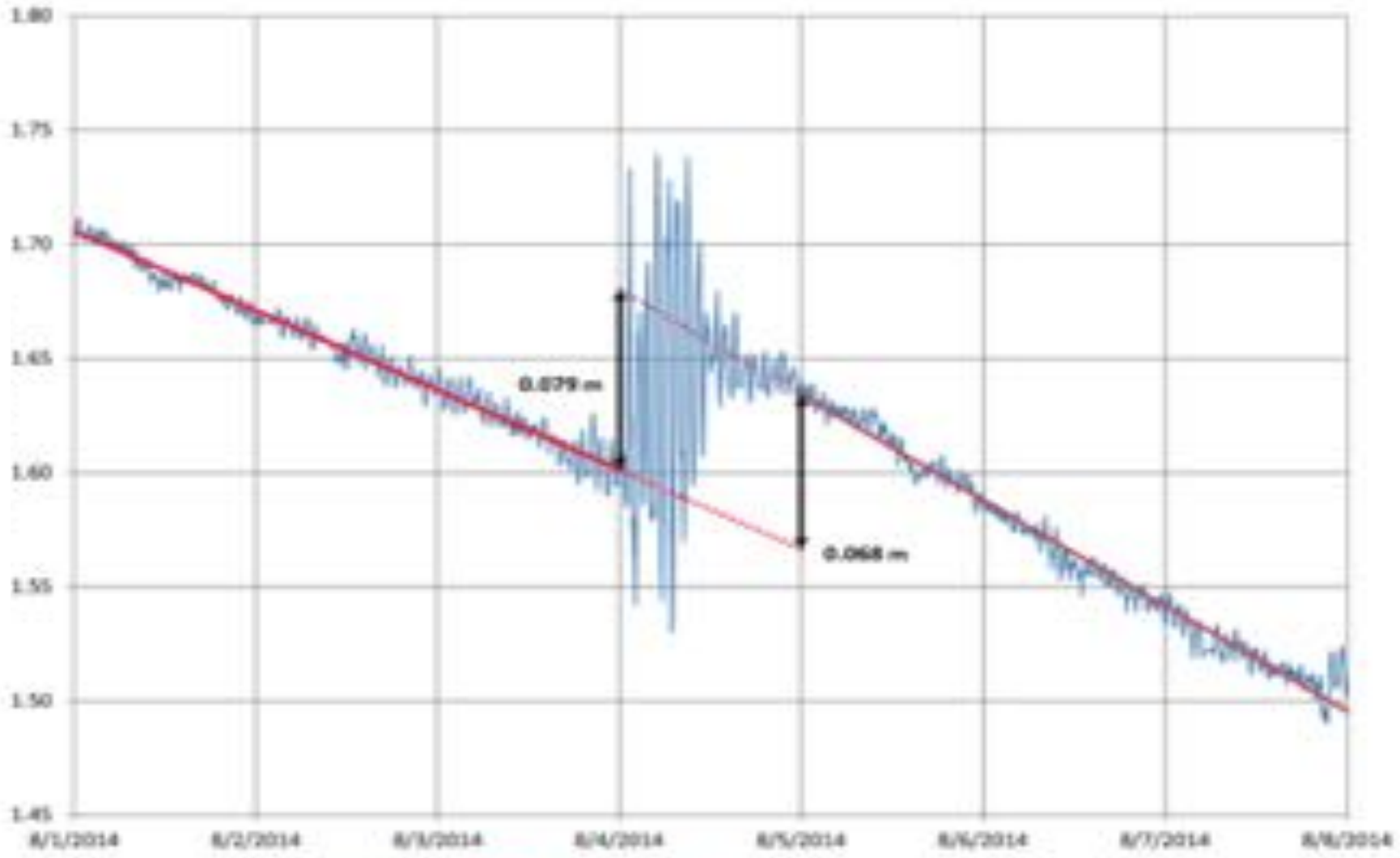


<https://www.youtube.com/watch?v=YJqDJZQU8E4>

# Subaqueous Gravity Flows in Quesnel Lake



Lake Water Level (m)



August 1-8 2014



GPS antenna

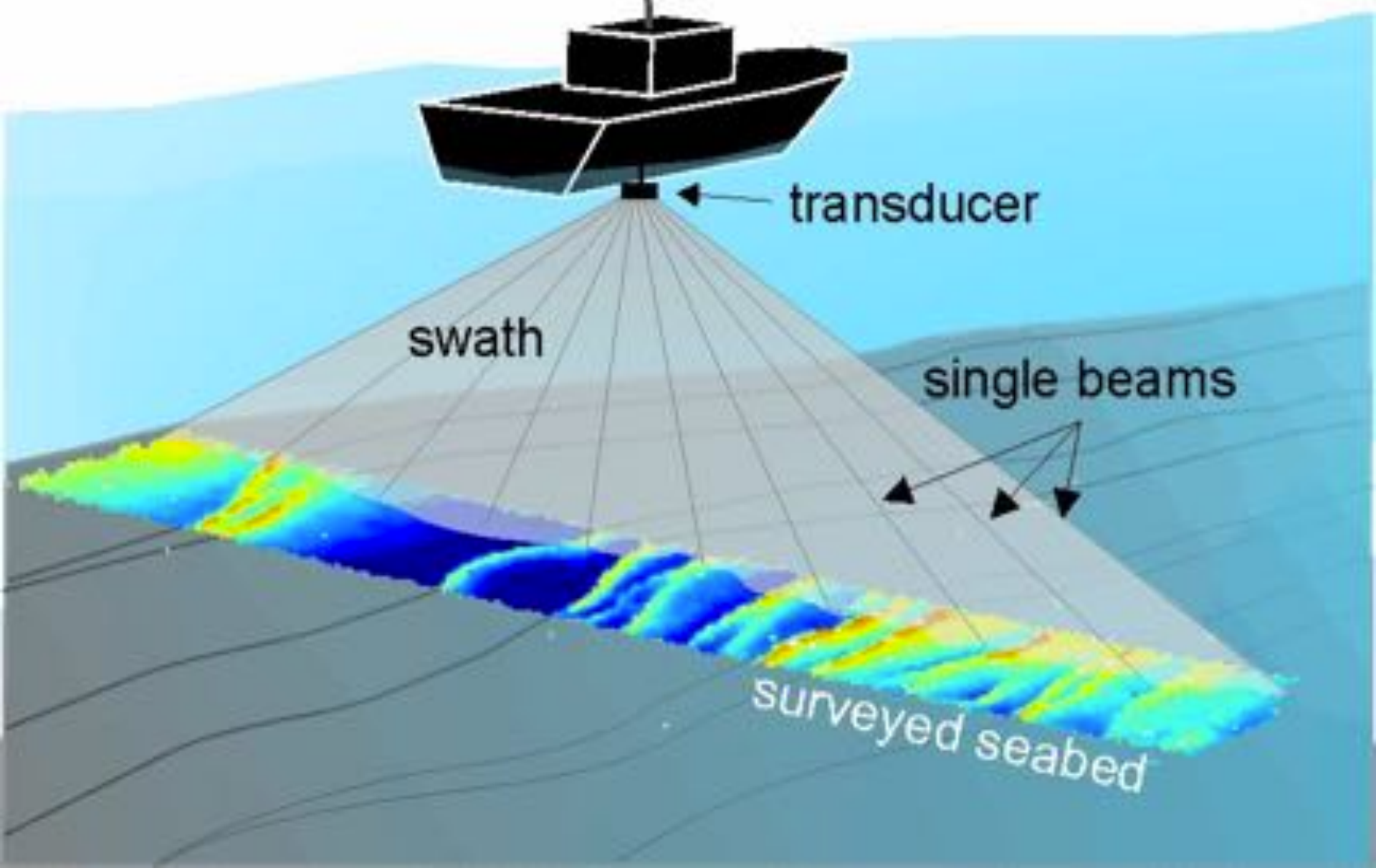


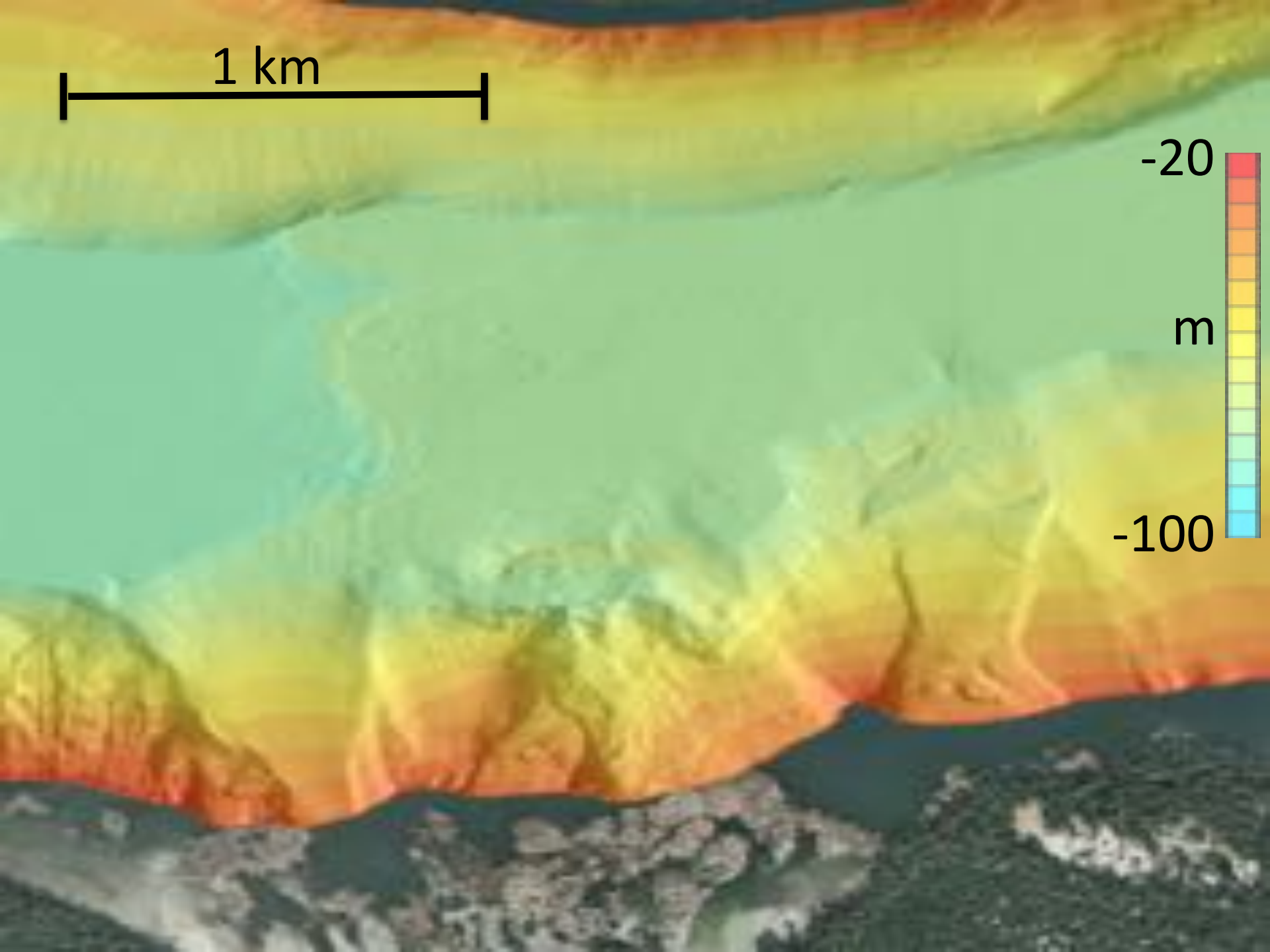
transducer

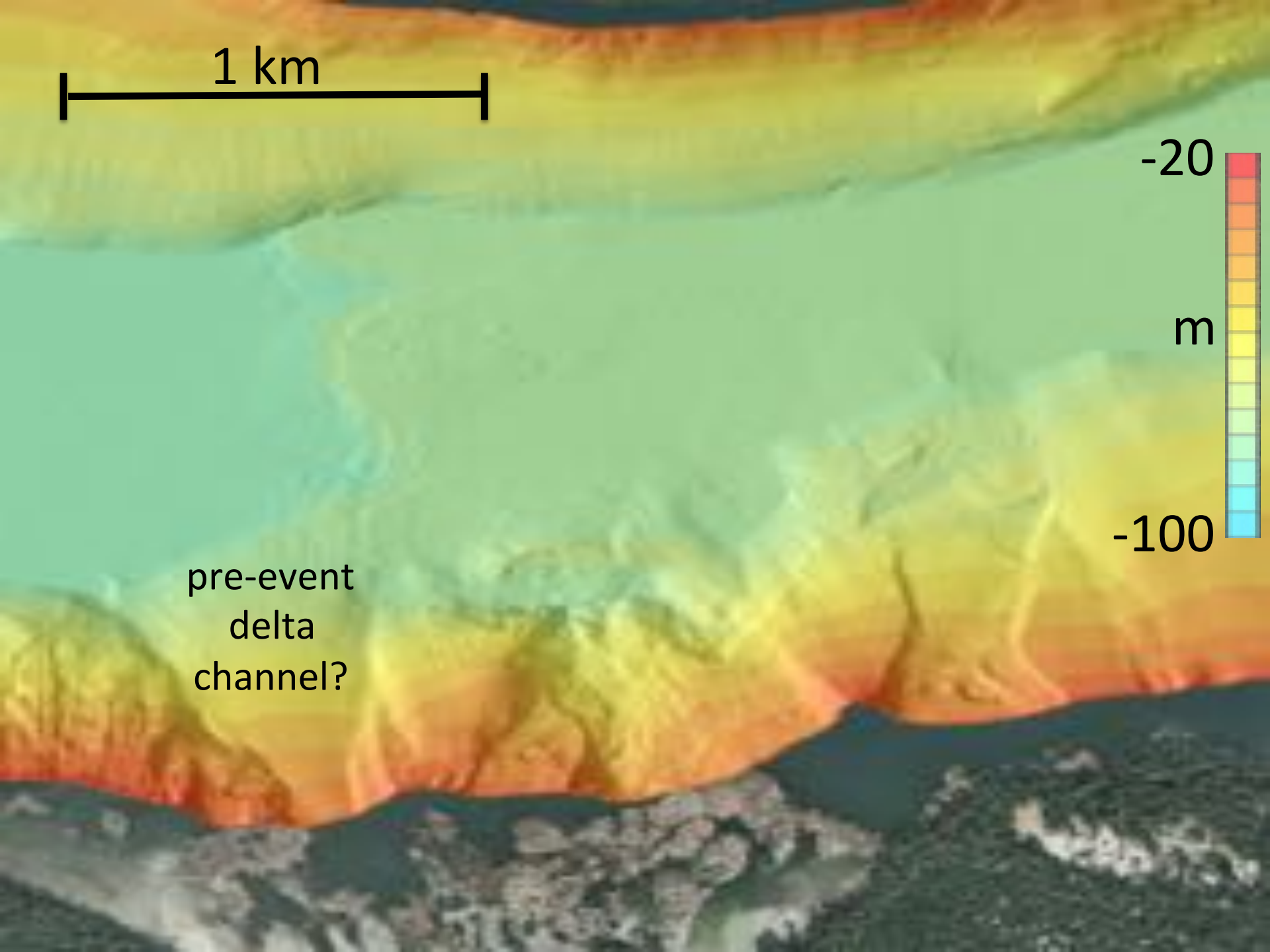
swath

single beams

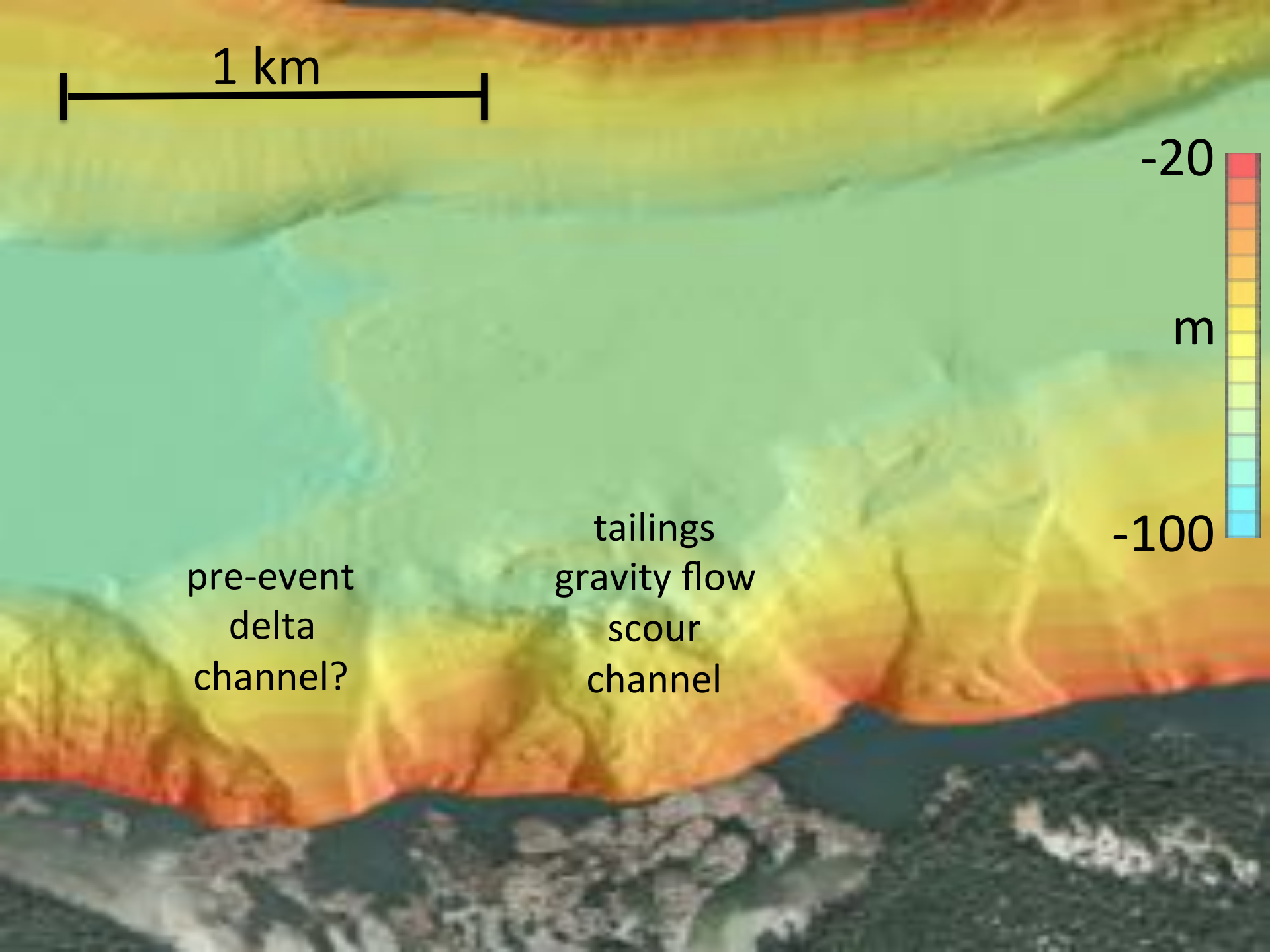
surveyed seabed











1 km

-20

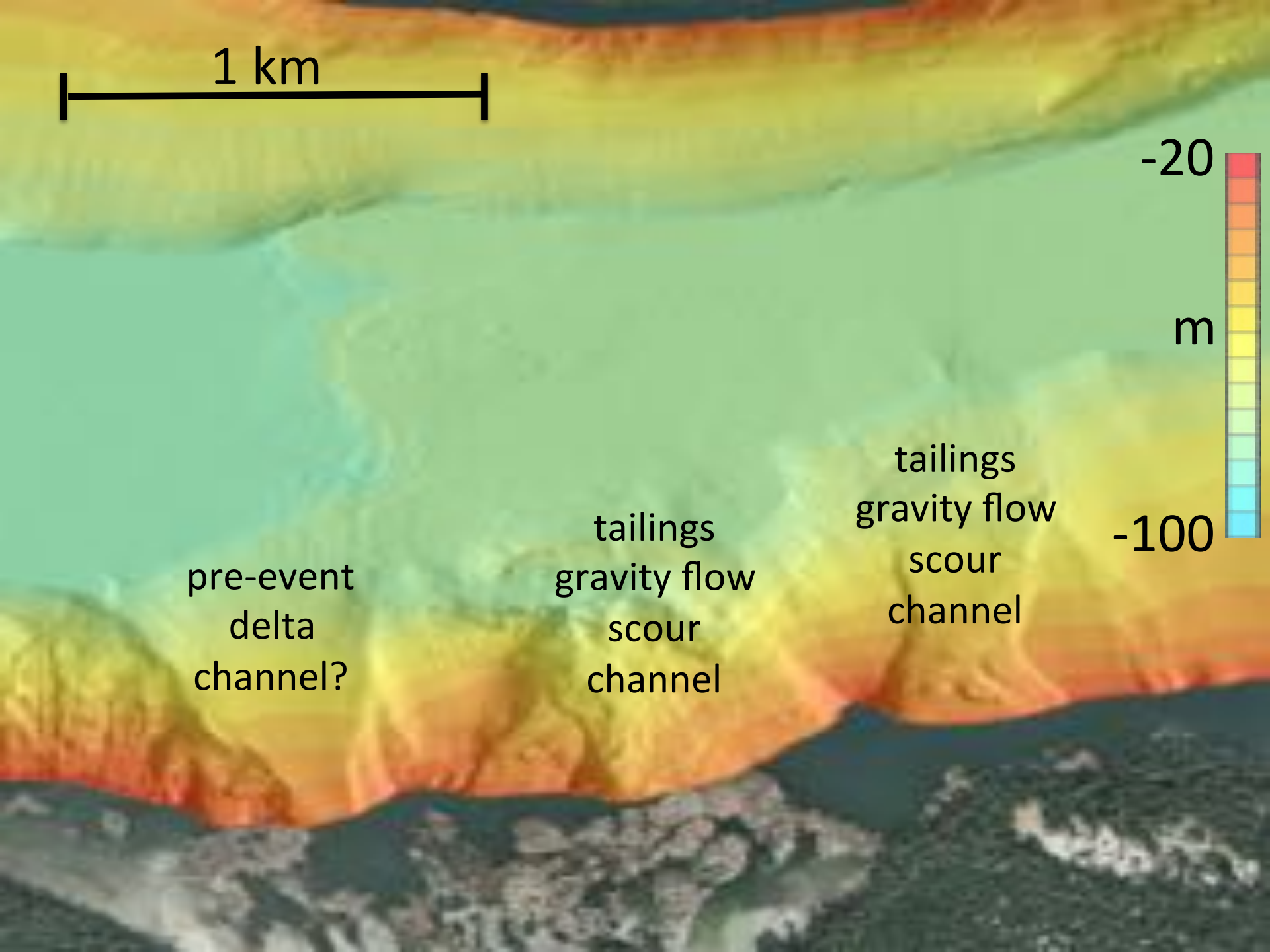
m

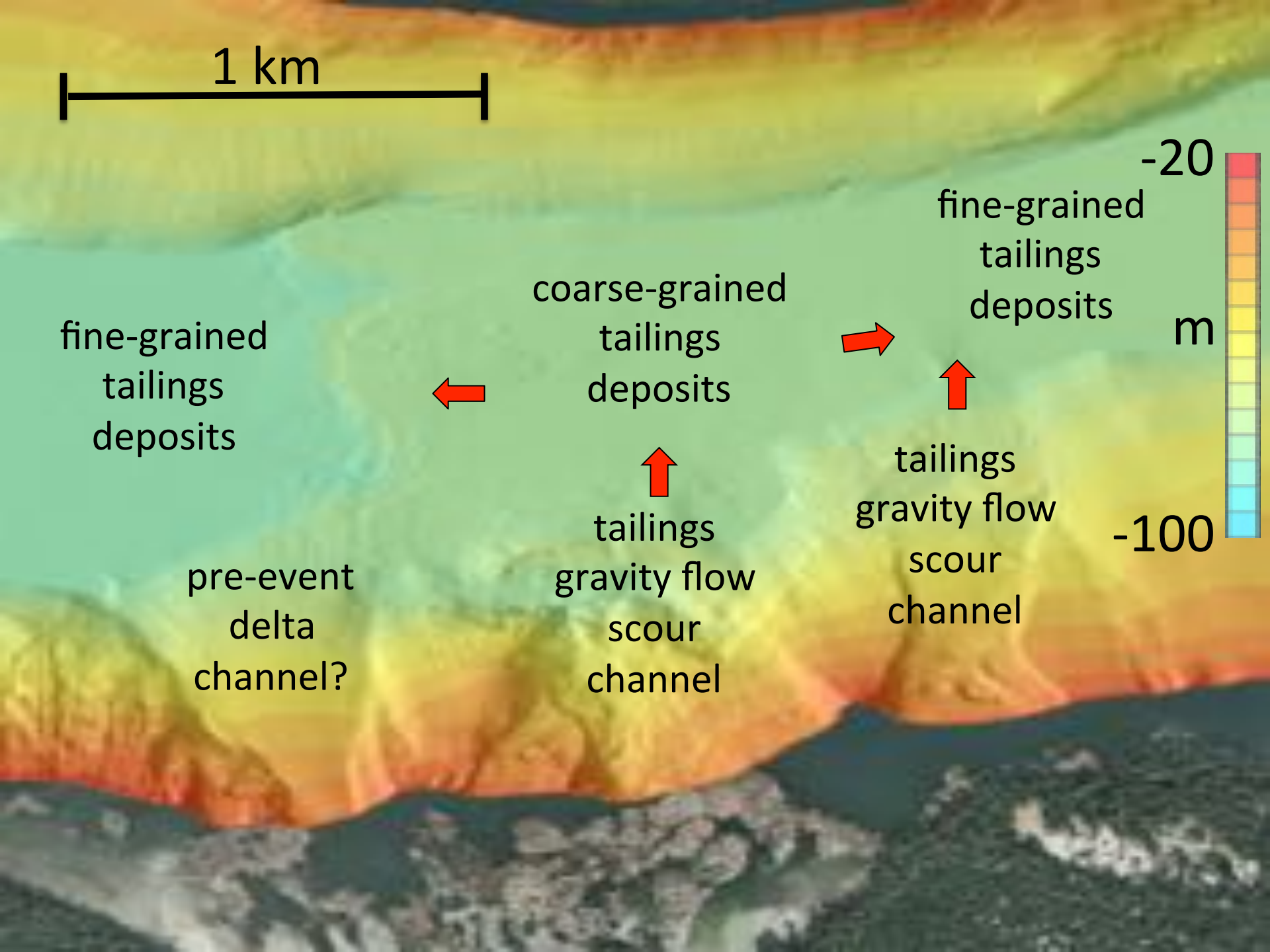
-100

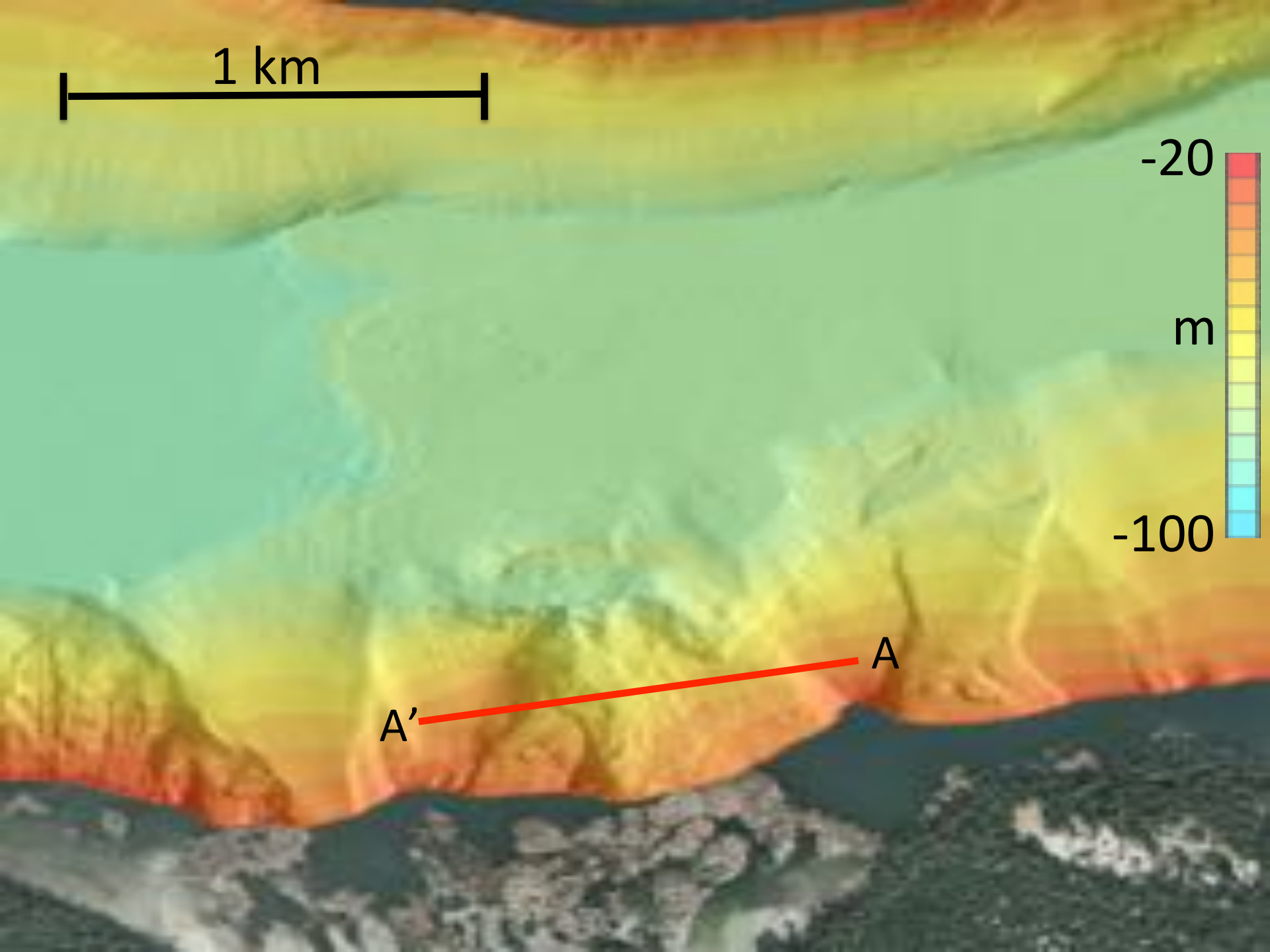
pre-event  
delta  
channel?

tailings  
gravity flow  
scour  
channel









1 km

-20

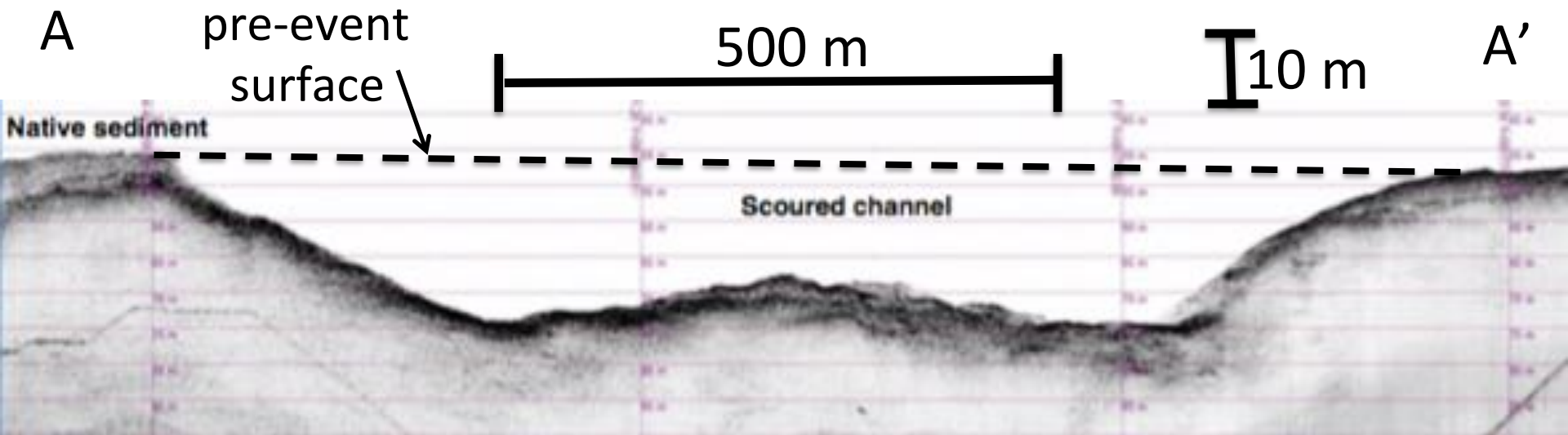
m

-100

A'


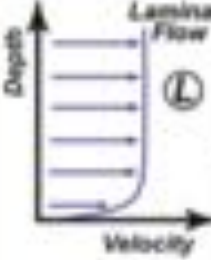
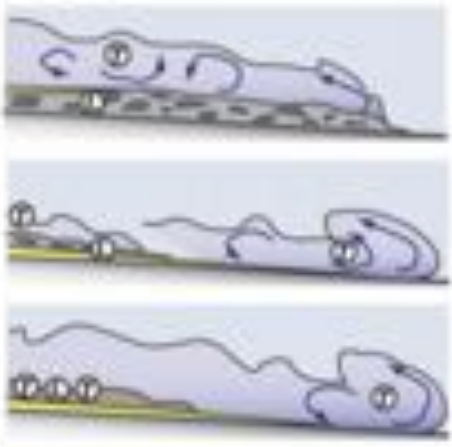


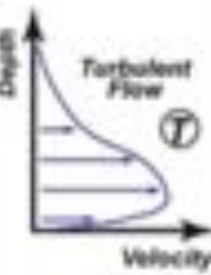

A

# Erosion by Subaqueous Debris Flows in Quesnel Lake

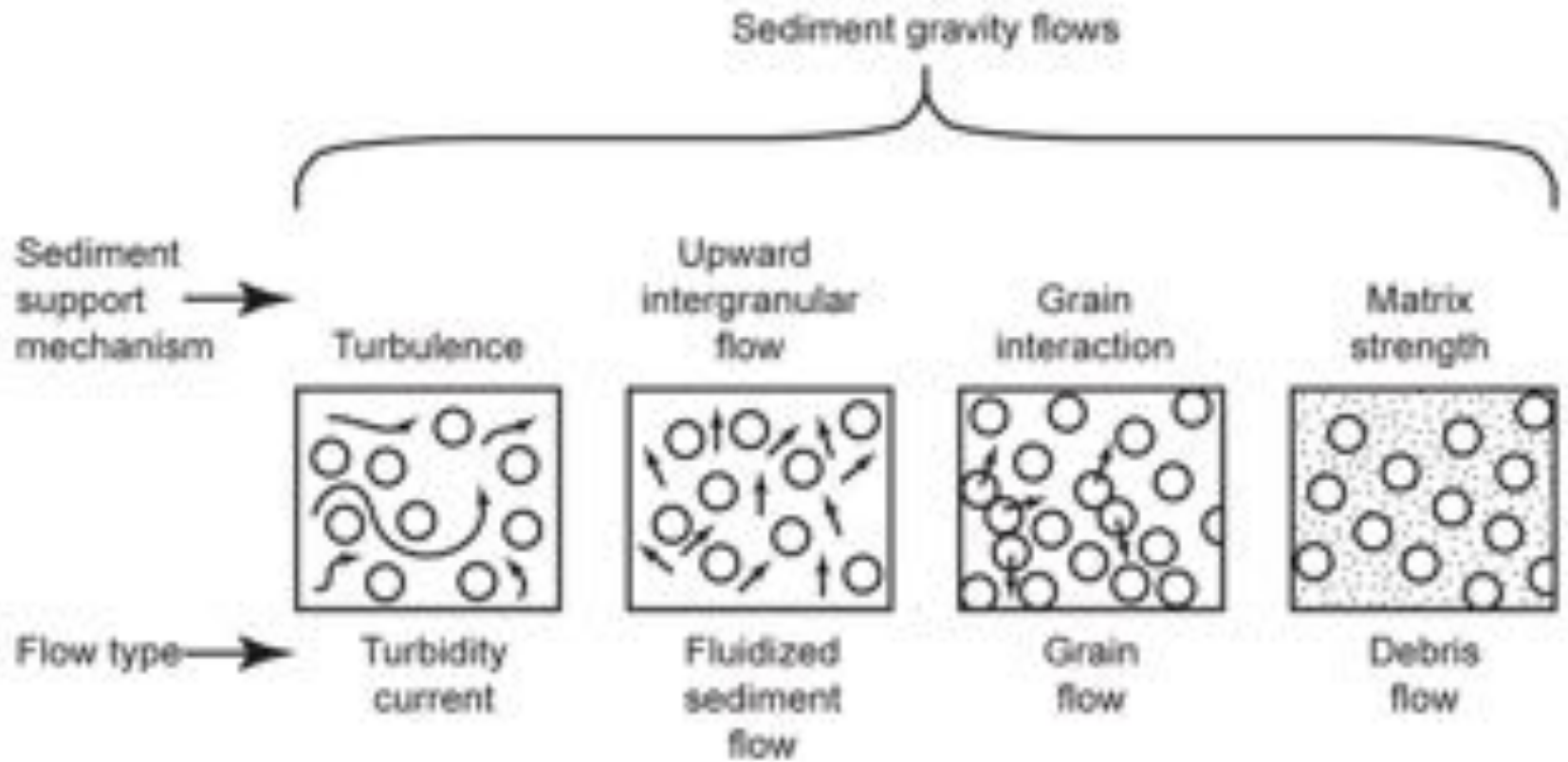


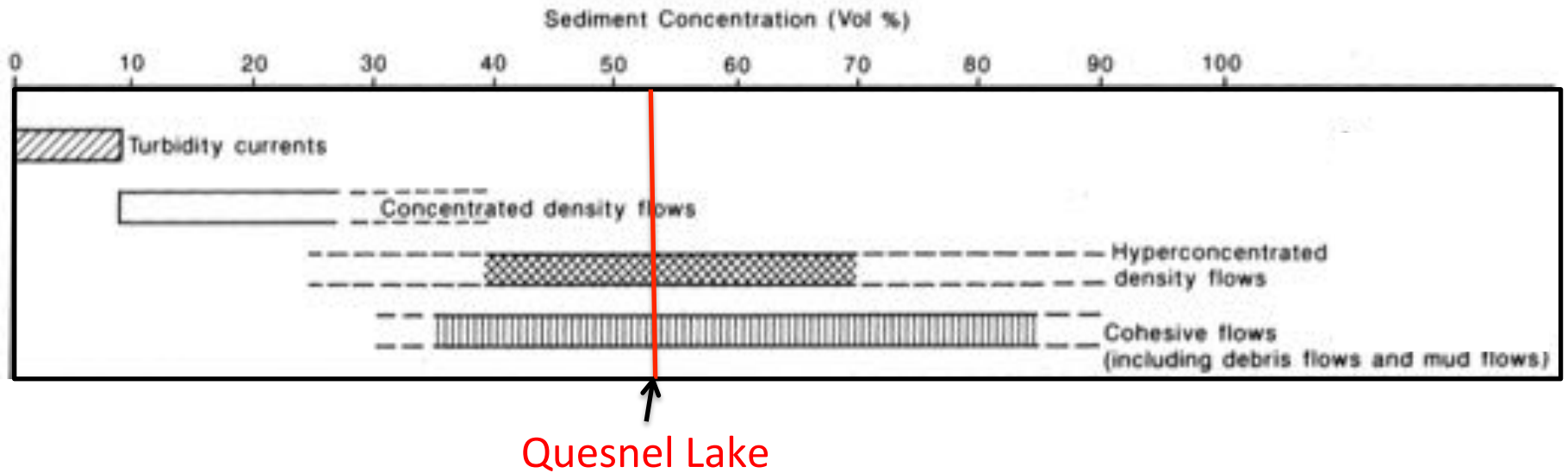


# Classification

FLOW TYPE		FLOW STRUCTURE	BEHAVIOUR
DEBRIS FLOW	CONVECTIVE		
COMPOSITE/ CO-GENETIC FLOWS	MIXED		
HIGH-DENSITY TURBIDITY CURRENT	NON-CONVECTIVE		
LOW-DENSITY TURBIDITY CURRENT			

Haughton et al. 2009, Marine and Petroleum Geology





Mulder et al. 2001, Sedimentology

# Erosion

- Up to 20 m vertical incision and  $1.5 \times 10^6 \text{ m}^3$  scoured in small cobbles and gravel on Hazeltine Creek fan-delta

JOURNAL OF GEOPHYSICAL RESEARCH, VOL. 117, F03006, doi:10.1029/2011JF002189, 2012

## **Elementary theory of bed-sediment entrainment by debris flows and avalanches**

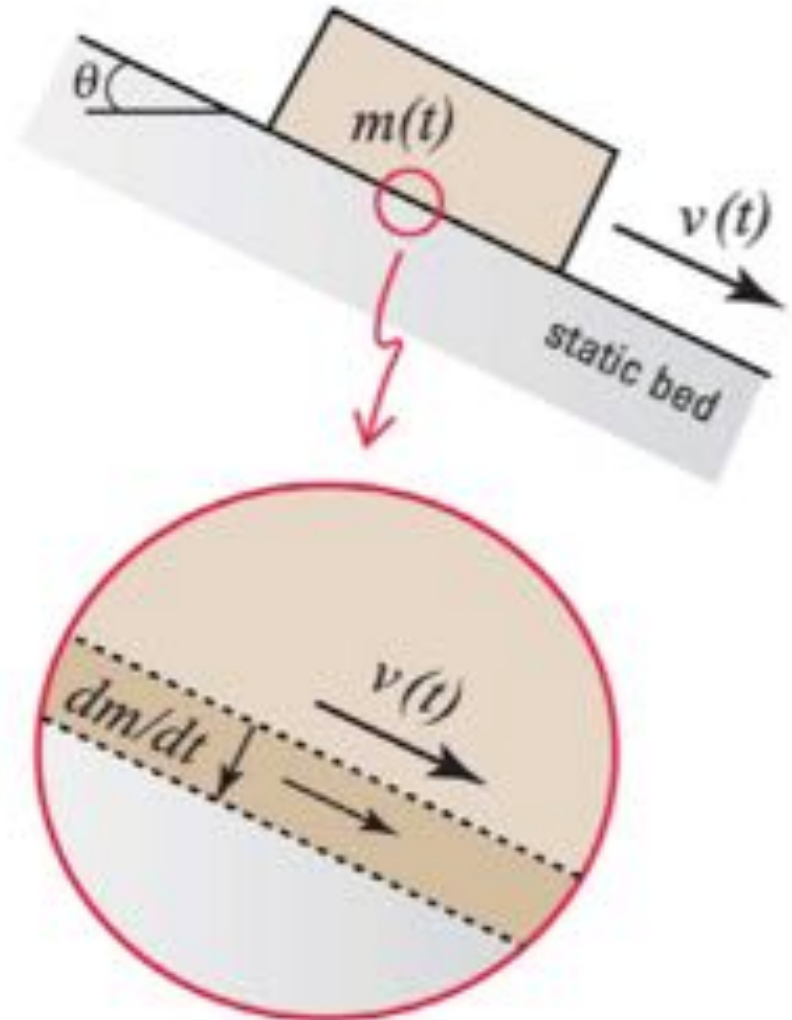
Richard M. Iverson<sup>1</sup>



# The Bare Bones of the Iverson model

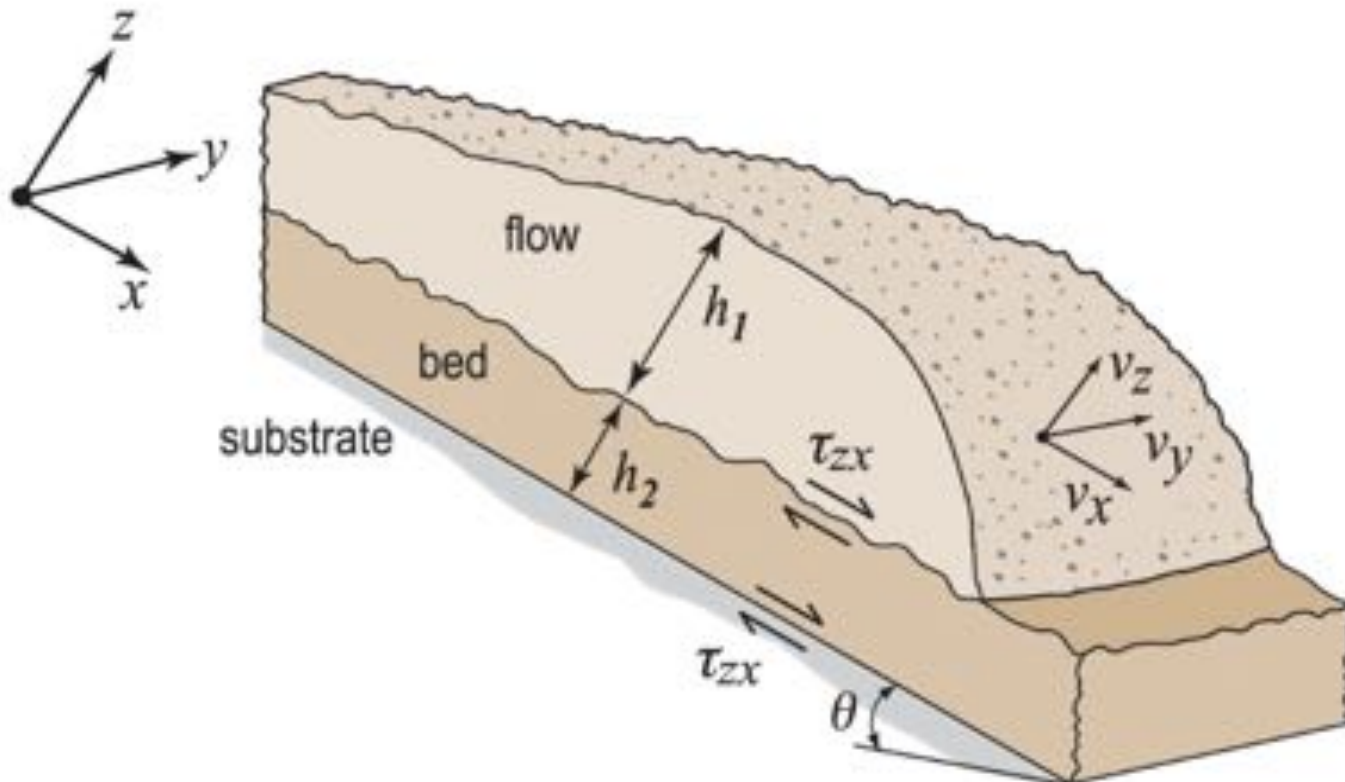
## Part 1:

- Coulomb slide block of mass  $m(t)$  and velocity  $v(t)$  descending a plane inclined at the angle  $\theta$



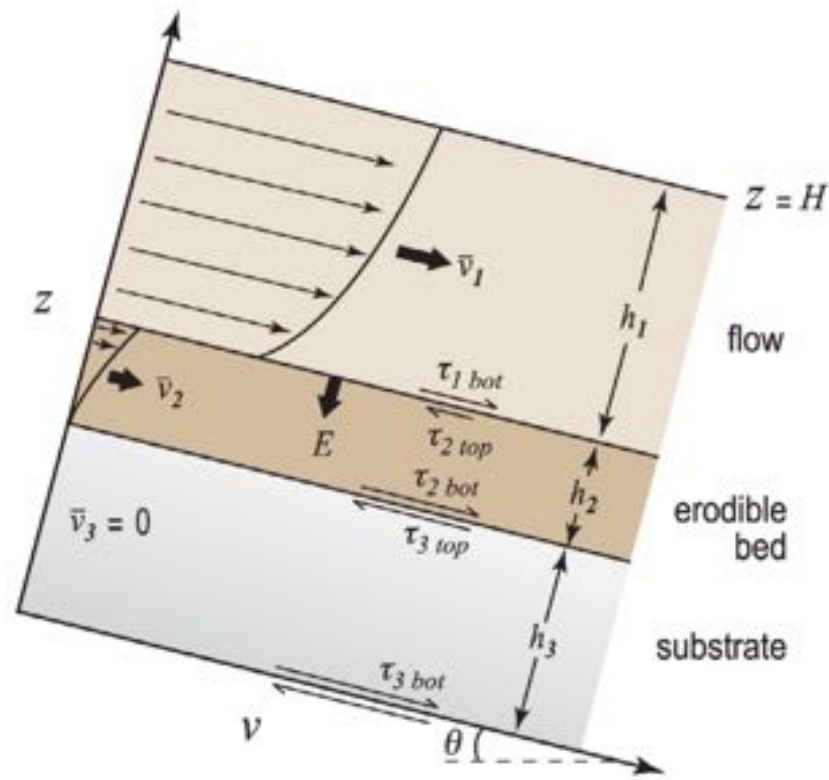
## Part 2:

- Three-layer, depth-integrated, continuum-mechanical model of mass and momentum exchange between a flow, an erodible bed, and a stable substrate.



- Part 2 model identifies mechanical controls on entrainment efficiency at the bed boundary
- Explicit predictions of the entrainment rate  $E$  result from making reasonable assumptions about flow velocity profiles and boundary shear tractions





$$E = \frac{\tau_{1bot} - \tau_{2top}}{\rho[(1 - s_1)\bar{v}_1 - v_{2top}]} \quad (34)$$

where:  $\tau$  is shear stress,  $\rho$  is the bulk density of the flow,  $s_1$  is a fitting parameter for the velocity profile in the flow,  $v$  is velocity

- Boundary shear tractions  $\tau_{1bot}$  and  $\tau_{2top}$  obey a Coulomb friction rule  $\tau = \mu \sigma'_{zz}$  where  $\mu$  is the Coulomb friction coefficient,  $\sigma'$  is effective normal stress:

$$\sigma'_{zz} = \sigma_{zz} - p, \quad (36)$$

- Boundary shear tractions that satisfy  $\tau = \mu \sigma'_{zz}$

$$\tau_{1bot} = \mu_1 (\sigma_{zz1bot} - p_{1bot}) = \mu_1 (\rho g h_1 \cos \theta - p_{1bot}), \quad (37)$$

$$\tau_{2top} = \mu_2 (\sigma_{zz2top} - p_{2top}) = \mu_2 (\rho g h_1 \cos \theta - p_{2top}), \quad (38)$$

where  $p$  is fluid pore pressure

- By incorporating (37) and (38), (34) becomes:

$$E = \frac{\rho g h_1 (\mu_1 - \mu_2) \cos \theta + \mu_2 p_{2 \text{ top}} - \mu_1 p_{1 \text{ bot}}}{(1 - s_1) \rho \bar{v}_1}. \quad (39)$$

- Contrasts in boundary pore fluid pressure can also promote entrainment
- If the top of the bed sediment becomes completely liquefied by high pore pressures (i.e.,  $p_{2 \text{ top}} = \rho g h_1 \cos \theta$ ) and the value  $s_1 = \frac{1}{2}$  is adopted to describe the flow velocity profile, then (39) reduces to:

$$E = \frac{2\mu_1 g h_1 \cos \theta (1 - \lambda_1)}{\bar{v}_1}, \quad (41)$$

where  $\theta$  is the slope angle,  $\mu_1$  is the flow's Coulomb friction coefficient,  $h_1$  is its thickness,  $v_1$  is its depth-averaged velocity, and  $\lambda_1$  is its degree of liquefaction:

$$\lambda_1 = p_{1bot} / \rho g h_1 \cos \theta \quad (42)$$



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- Is there anything counterintuitive about (41)?

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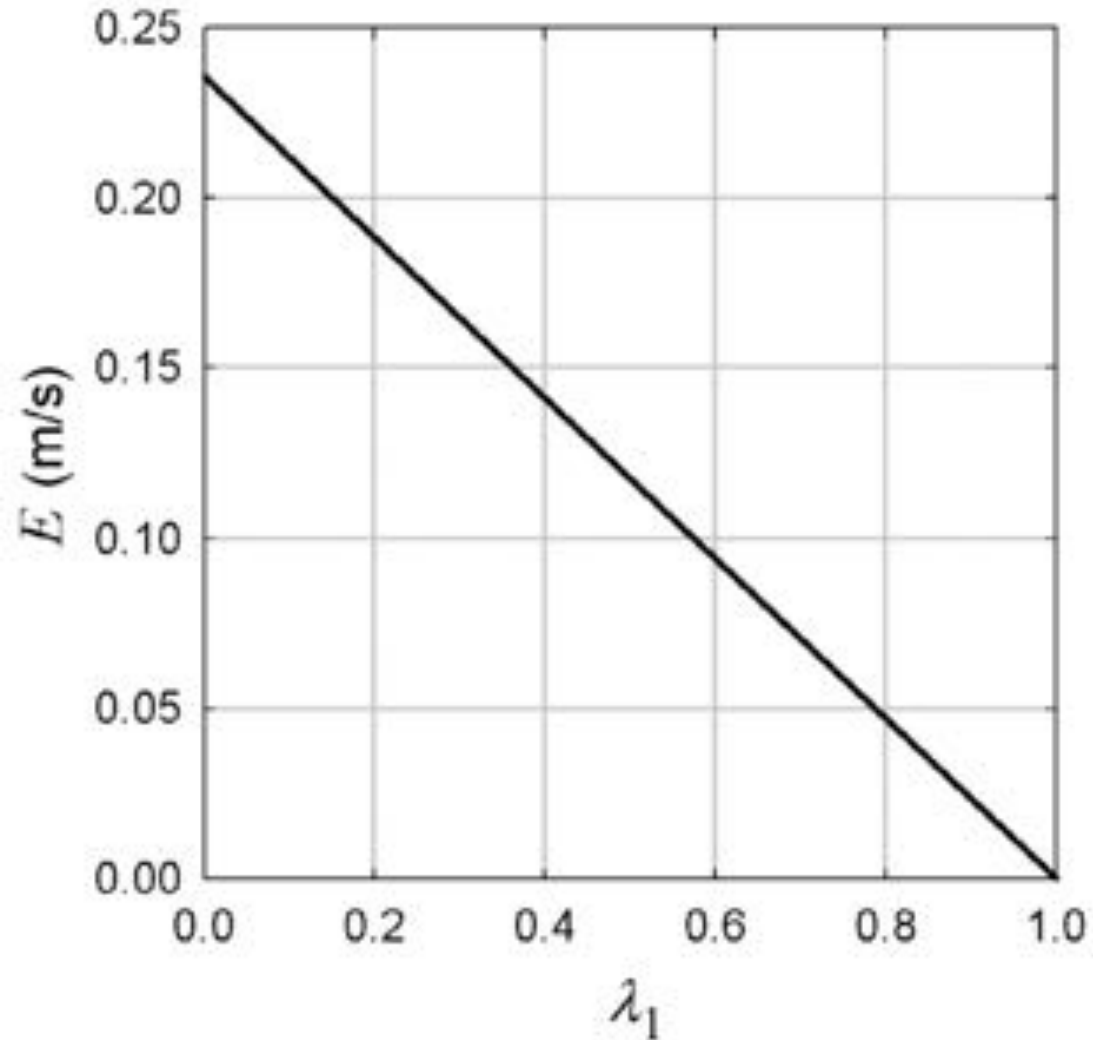
$$E \propto 1/v_{1bot}$$

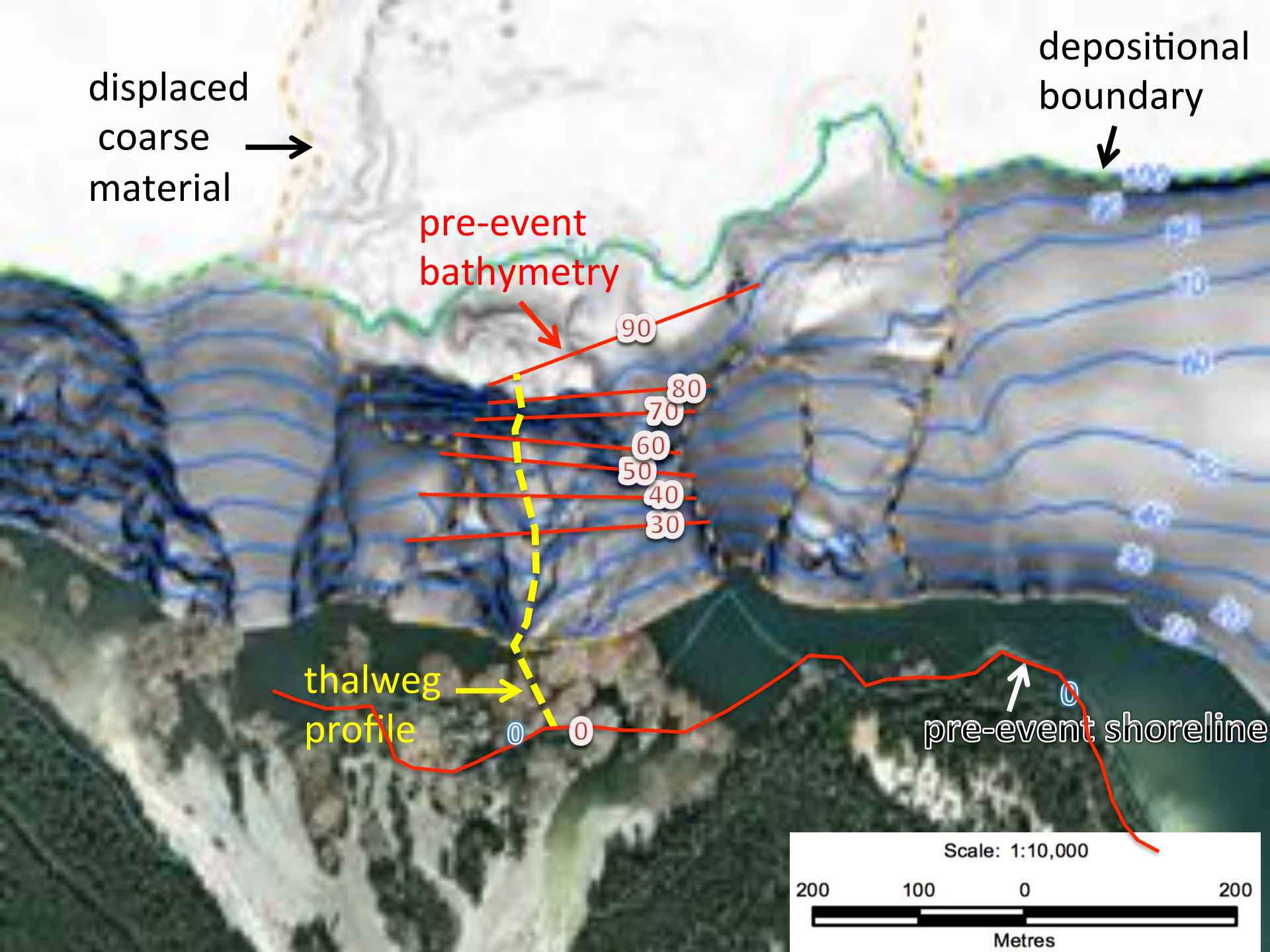


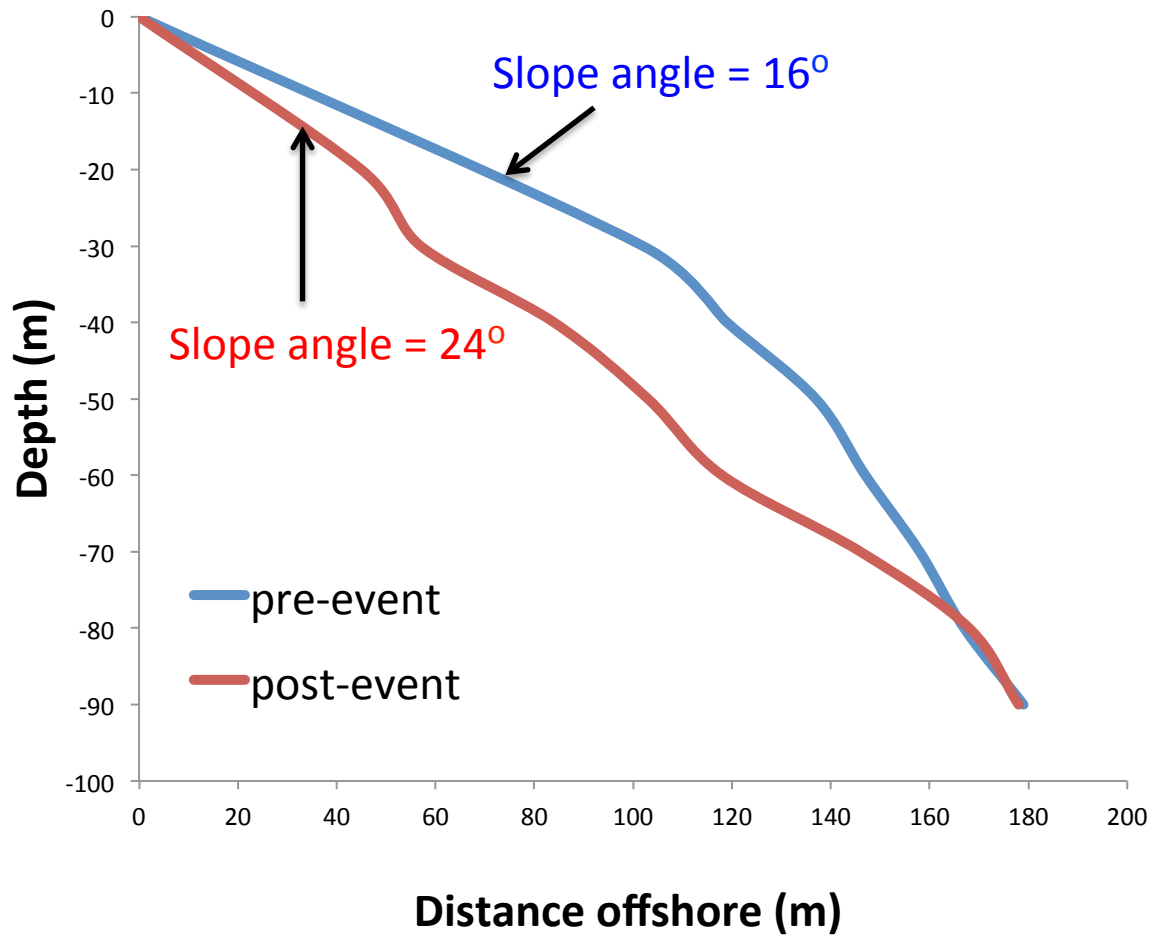




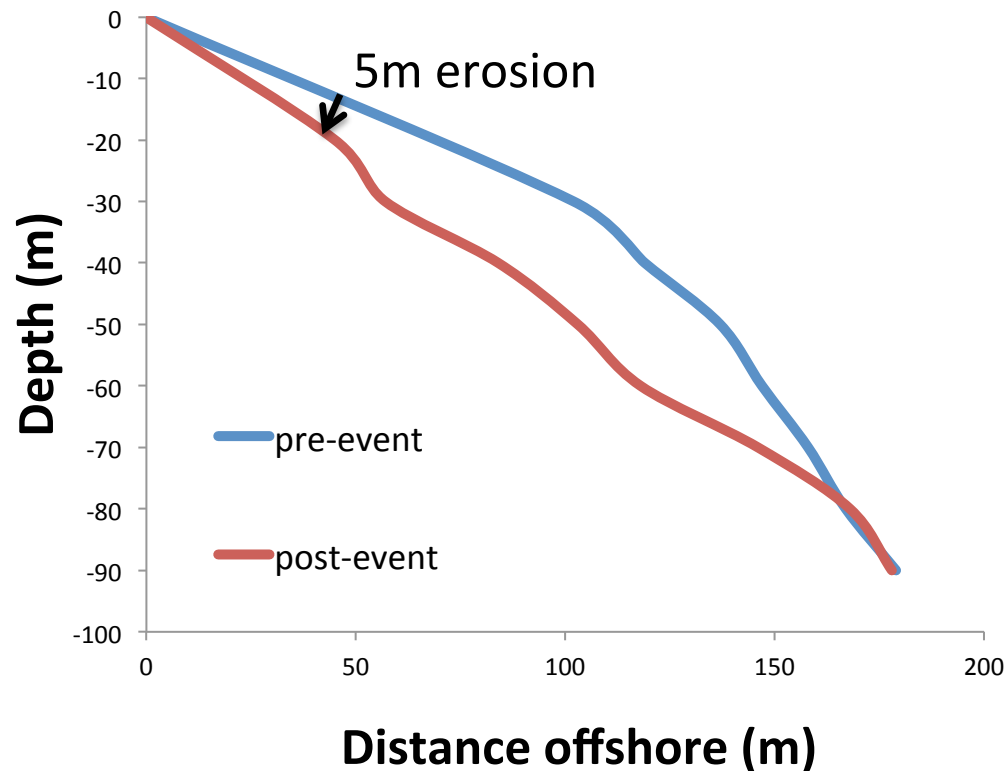
- Flow liquefaction likely plays a critical role in bed entrainment







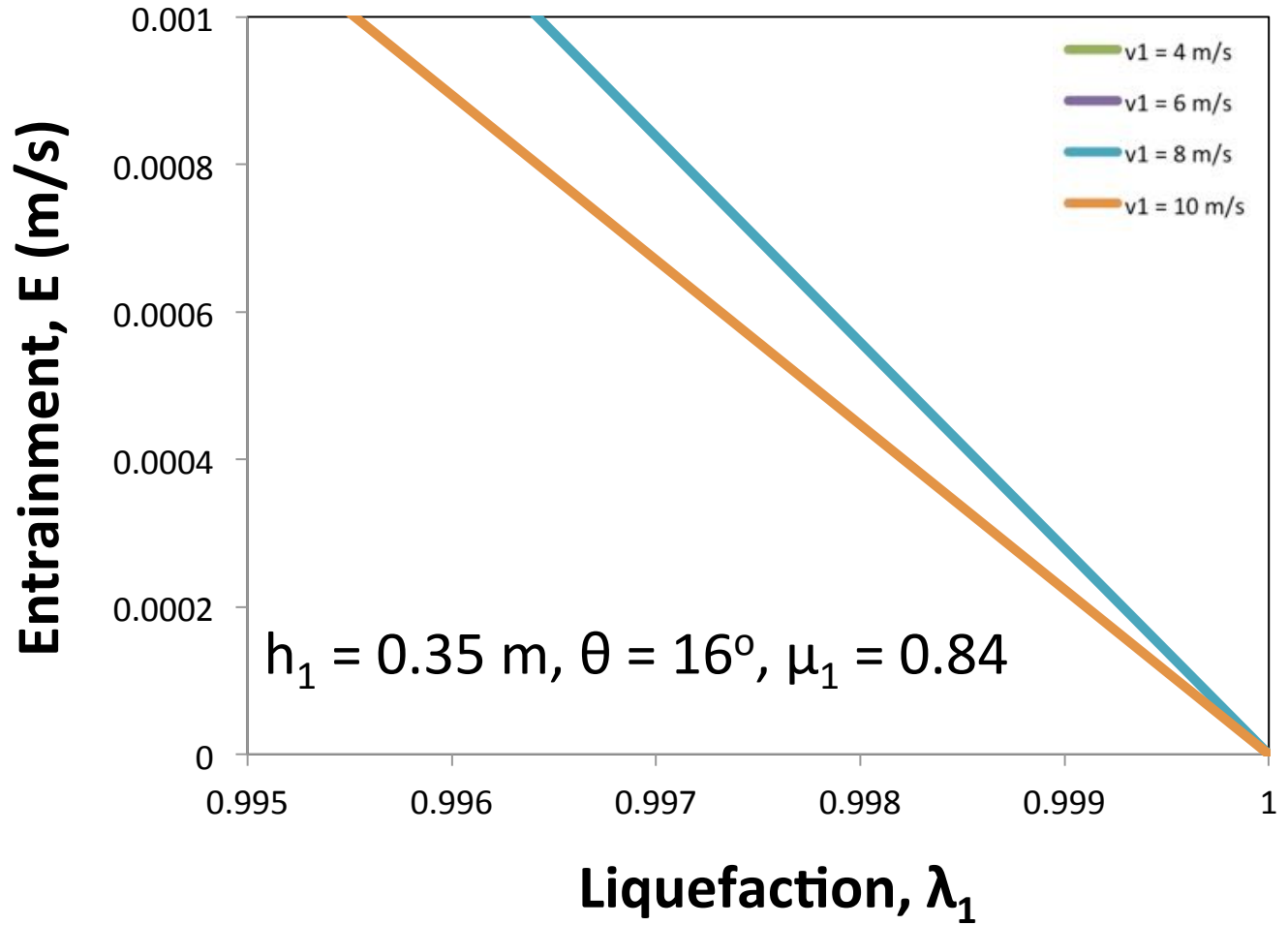
- Test case: measured erosion rate,  $E_m$ , for 5 m of scour in the large scour channel:



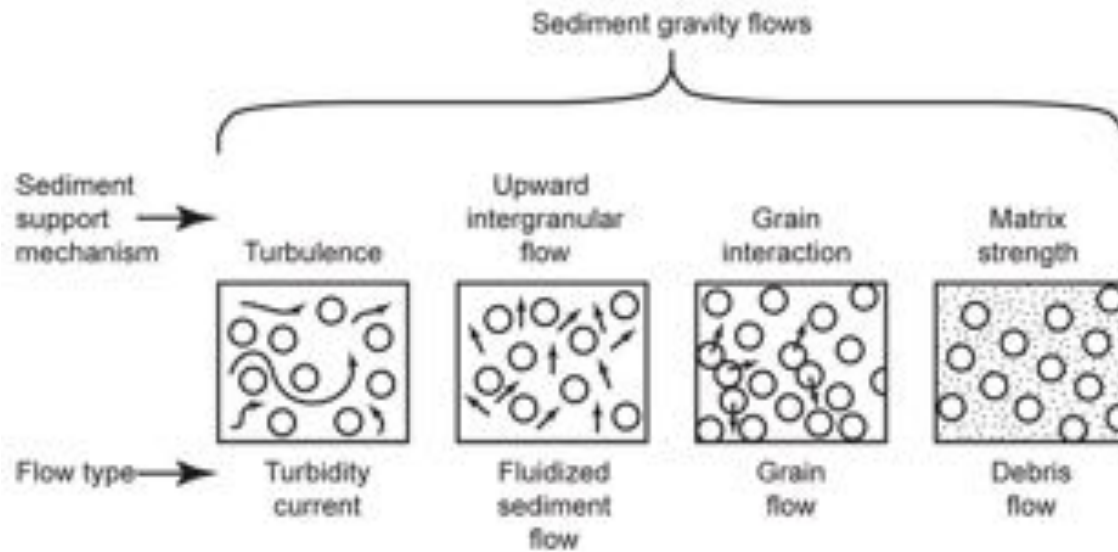
<b>Duration (hours)</b>	12	8	6
<b><math>E_m</math> (m/s)</b>	0.0001157	0.0001736	0.0002314



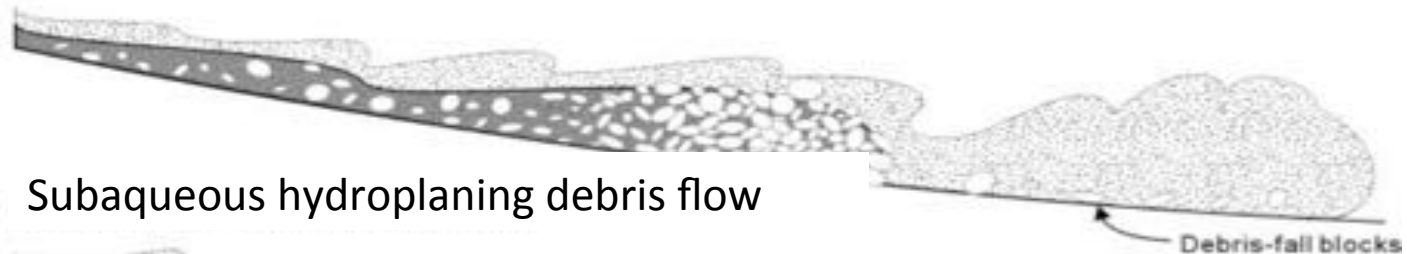
- Suberial debris flow thickness at Hazeltine Creek mouth is estimated at  $h_1 = 0.35$  m
- Gradient of Hazeltine Creek fan-delta near creek mouth is  $\theta = 16^\circ$
- In experimental and natural subaerial debris flows:
  - $\mu_1 = 0.84 - 0.97$
  - $\lambda_1 = 0.5 - 0.8$
  - $v_1 = 3.9 - 12$  m/s



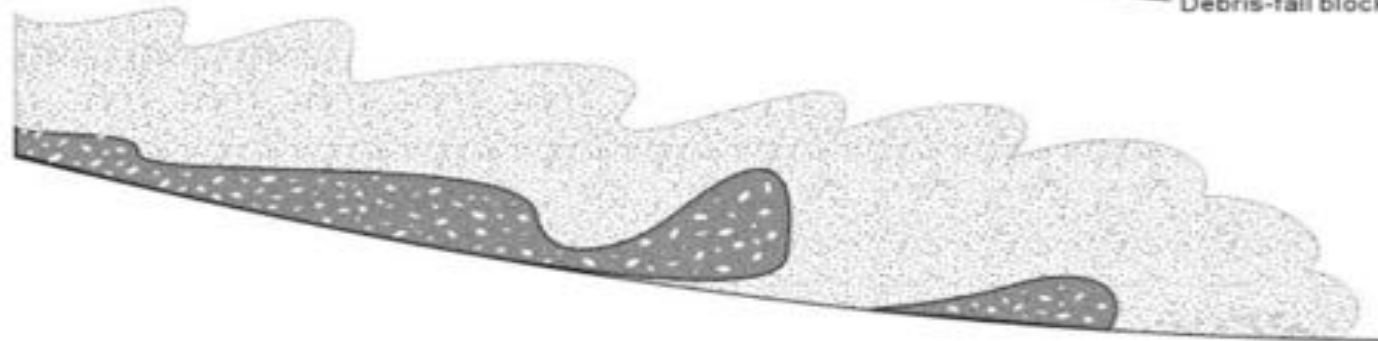




Subaqueous non-hydroplaning debris flow



Subaqueous hydroplaning debris flow





# Summary so far...

- Failure of the Mt. Polley mine tailings dam caused  $14 \times 10^6 \text{ m}^3$  of sediment and interstitial water to flow into Quesnel Lake
- The resulting subaqueous debris flow in Quesnel Lake eroded  $1.5 \times 10^6 \text{ m}^3$  of fan-delta fine cobbles and gravel
- A test case of the Iverson (2012) debris flow entrainment model suggests that the erosional debris flows in Quesnel Lake were nearly liquefied

# What now?

- Carry on with Iverson model



Go for  
it!

- A different approach/model?
  - Sedflux (Hutton and Syvitski 2008)
  - Suggestions?

But wait, there's more!









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## Dark Universe

journal homepage: [www.elsevier.com/locate/agee](http://www.elsevier.com/locate/agee)



# Dark matter debris flows in the Milky Way

Mariangela Lisanti<sup>a,\*</sup>, David N. Spergel<sup>b</sup>

<sup>a</sup> Princeton Center for Theoretical Science, Princeton University, Princeton, NJ 08544, USA

<sup>b</sup> Department of Astrophysical Sciences, Princeton University, Princeton, NJ 08540, USA

