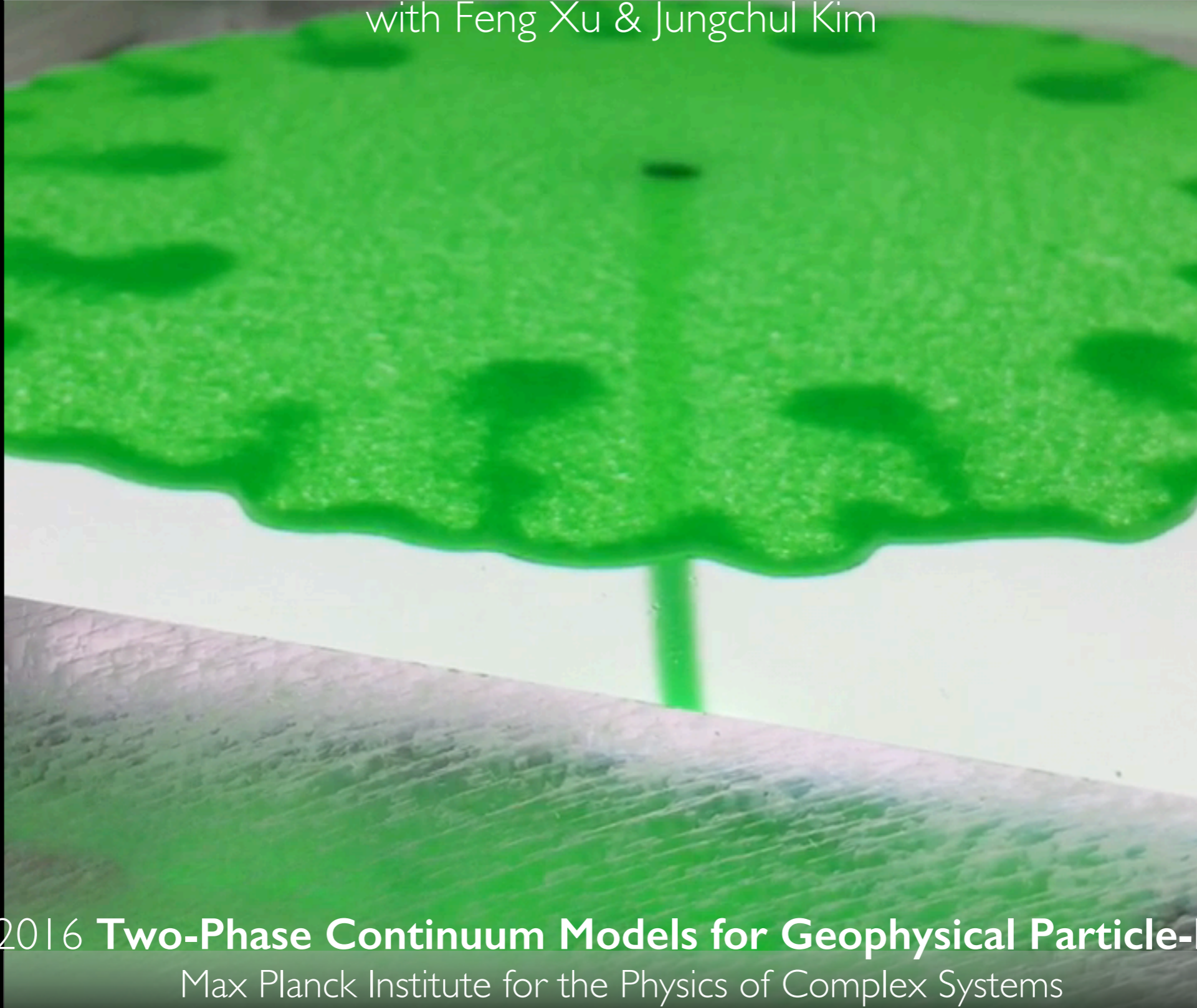


PARTICLE-INDUCED FINGERING



Sungyon Lee Mechanical Engineering, Texas A&M

with Feng Xu & Jungchul Kim



03.14-18.2016 **Two-Phase Continuum Models for Geophysical Particle-Fluid Flows**

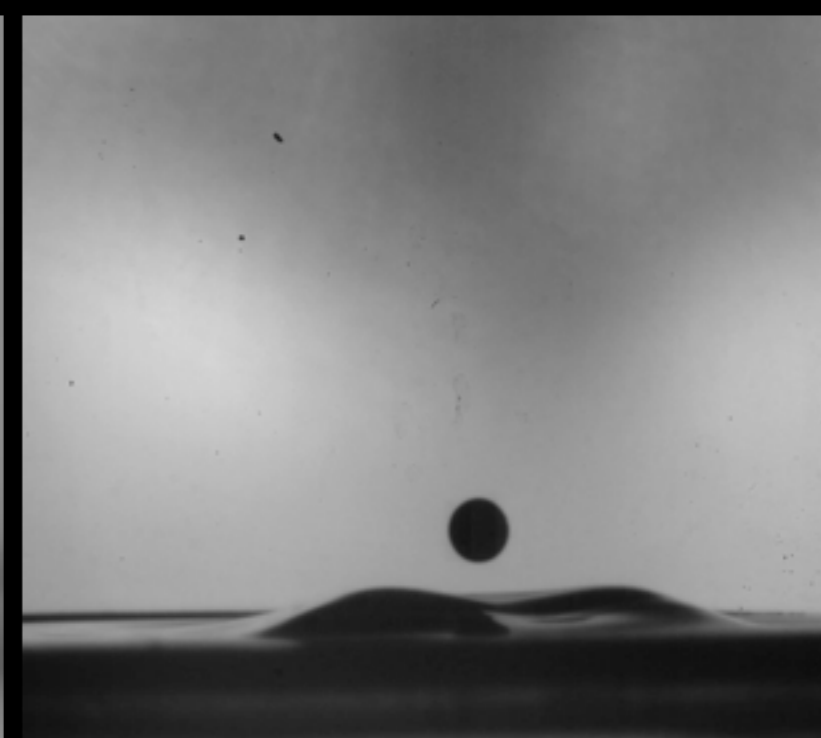
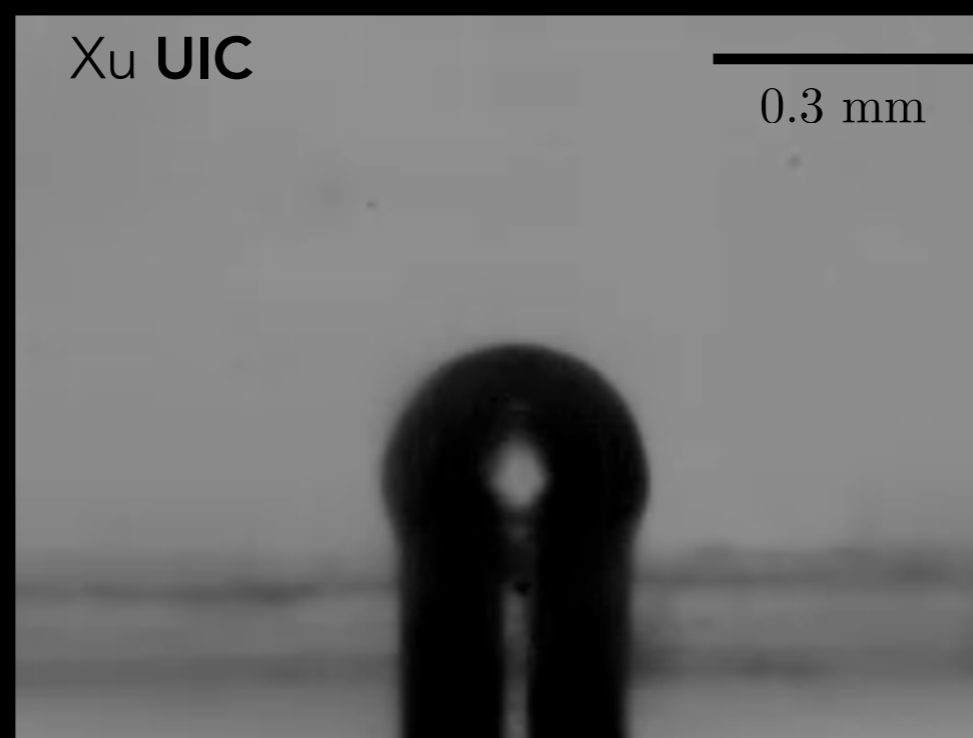
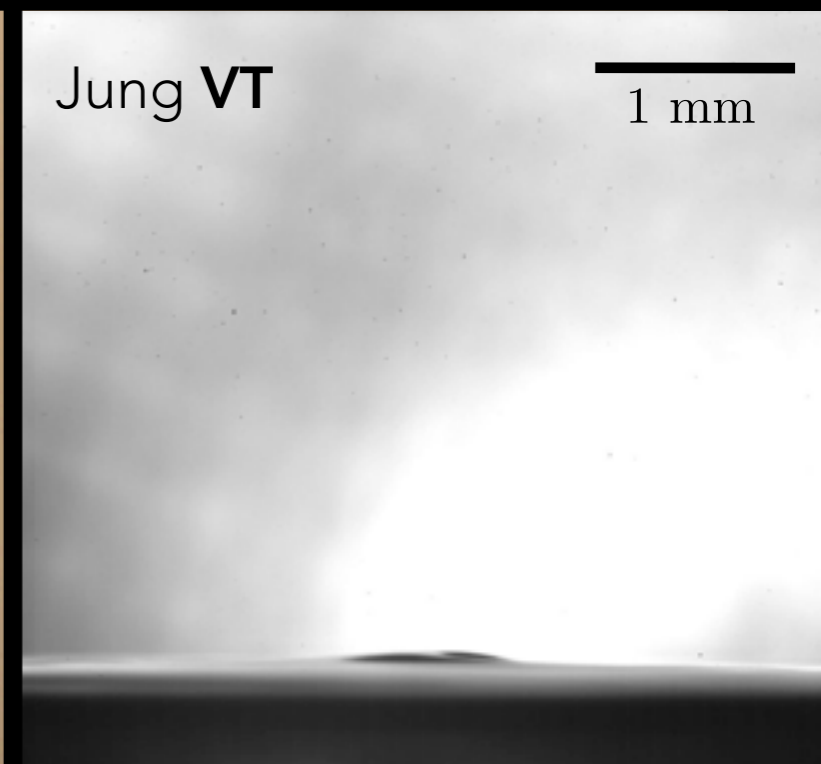
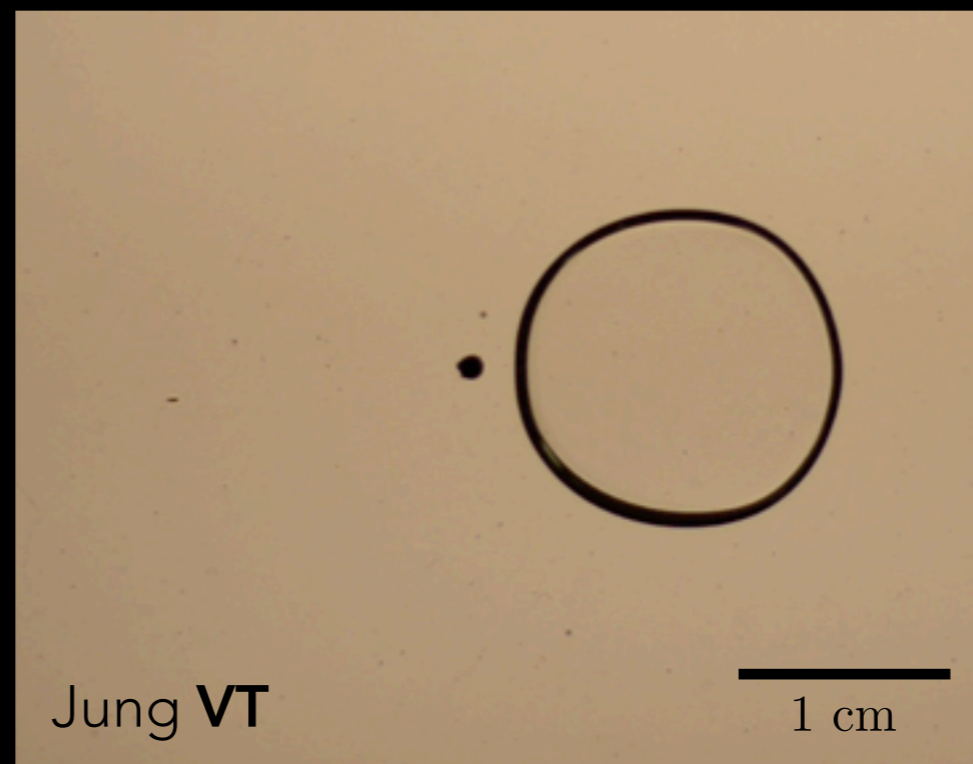
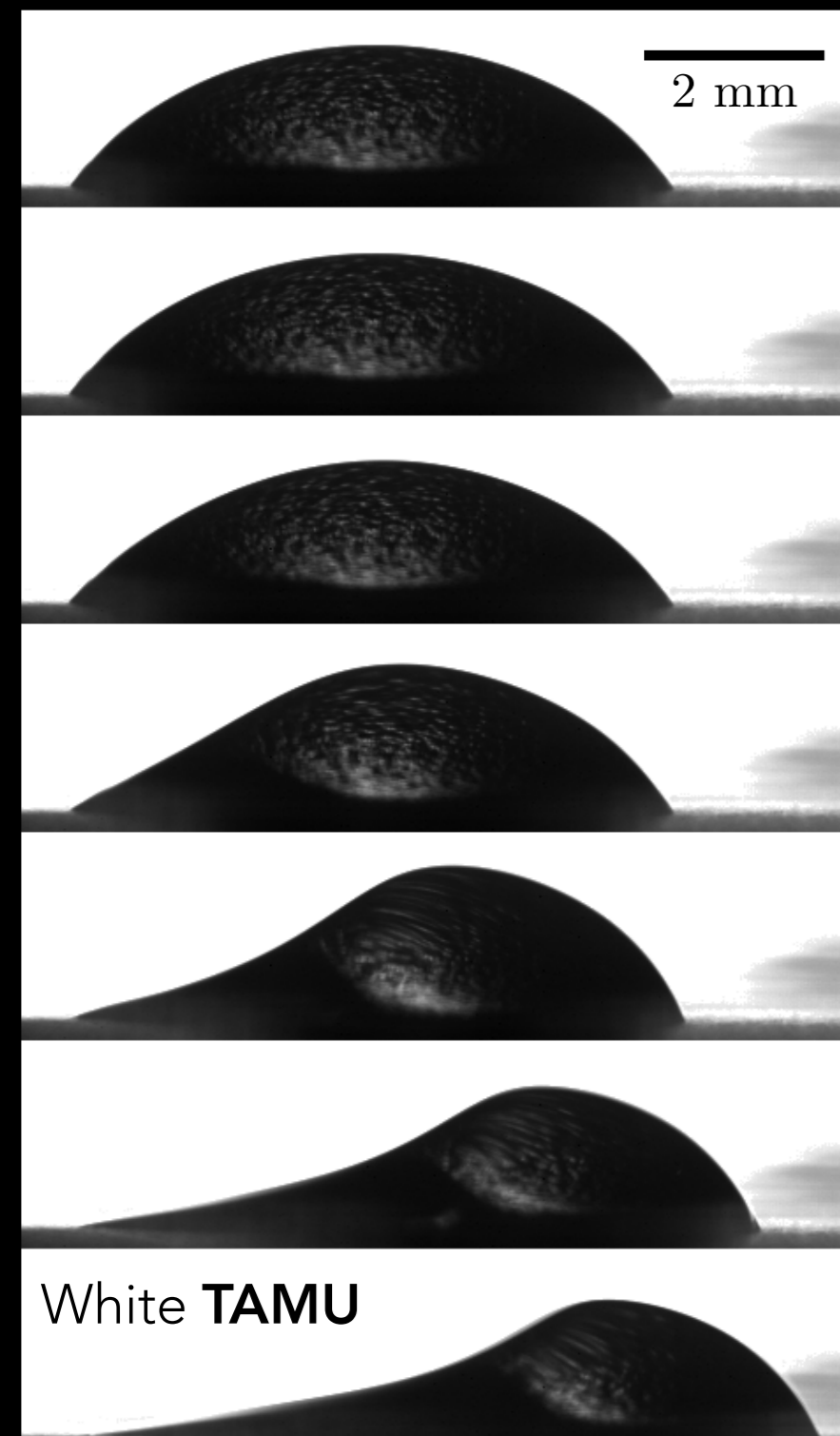
Max Planck Institute for the Physics of Complex Systems

BUT FIRST....



DrIPs

DROPS, INTERFACES & PARTICULATE SYSTEMS

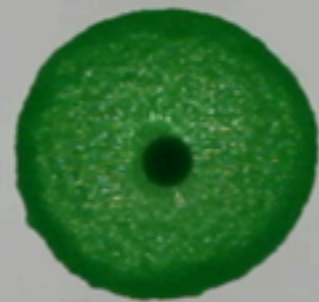


We study **interfacial** dynamics.

DrIPs

DROPS, INTERFACES & PARTICULATE SYSTEMS

particle-induced viscous fingering



5 cm

bubbles in porous media



MacMinn
Oxford

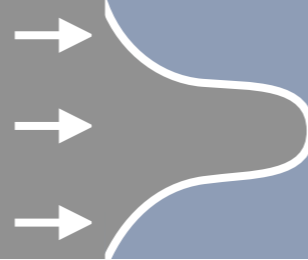
2 cm

We also like **particles**...

VISCOUS FINGERING

"invading" phase

μ_i

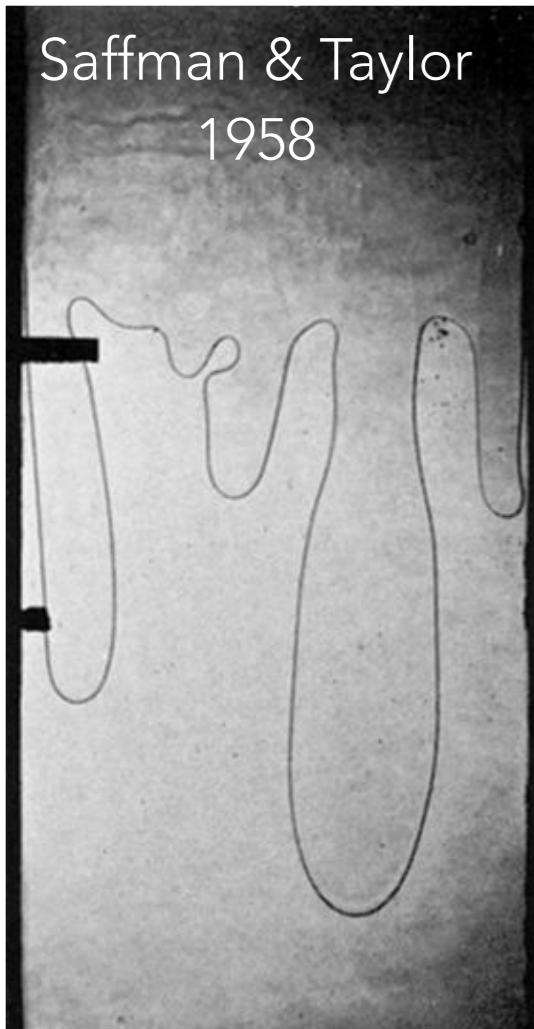


"defending" phase

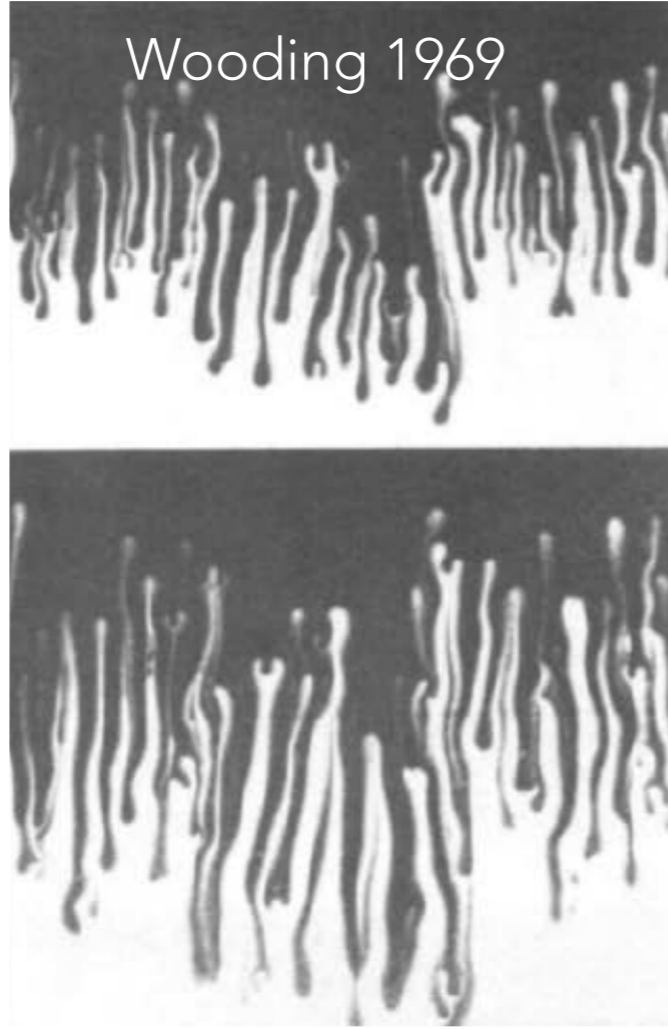
μ_d

Interface is **unstable** when $\mu_i < \mu_d$.

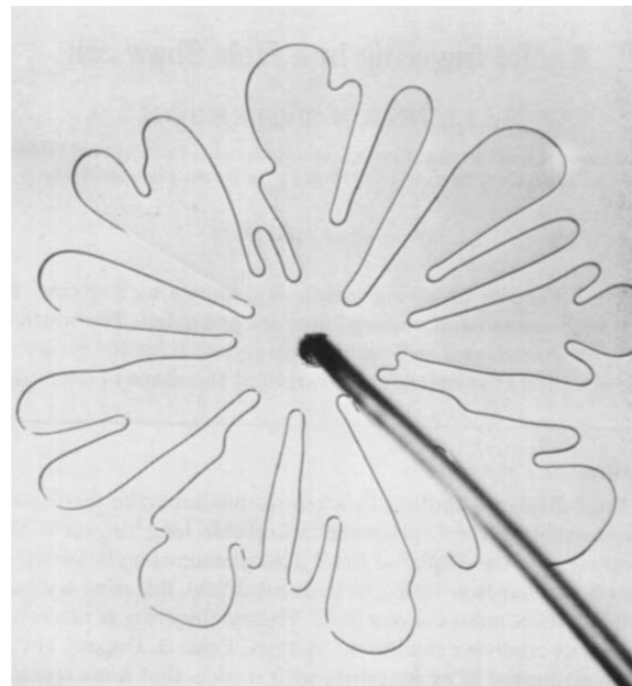
Saffman & Taylor
1958



Wooding 1969



Paterson 1981

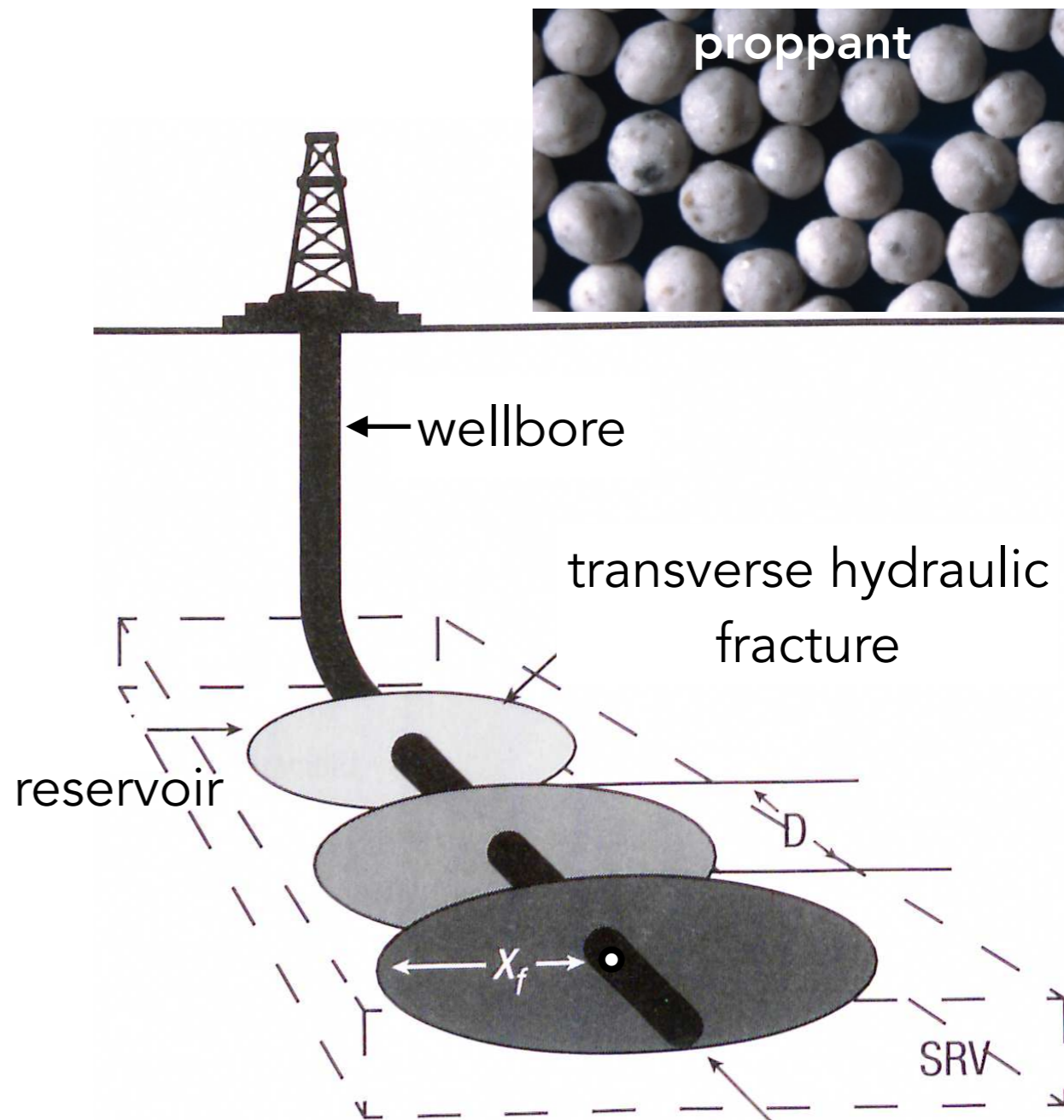
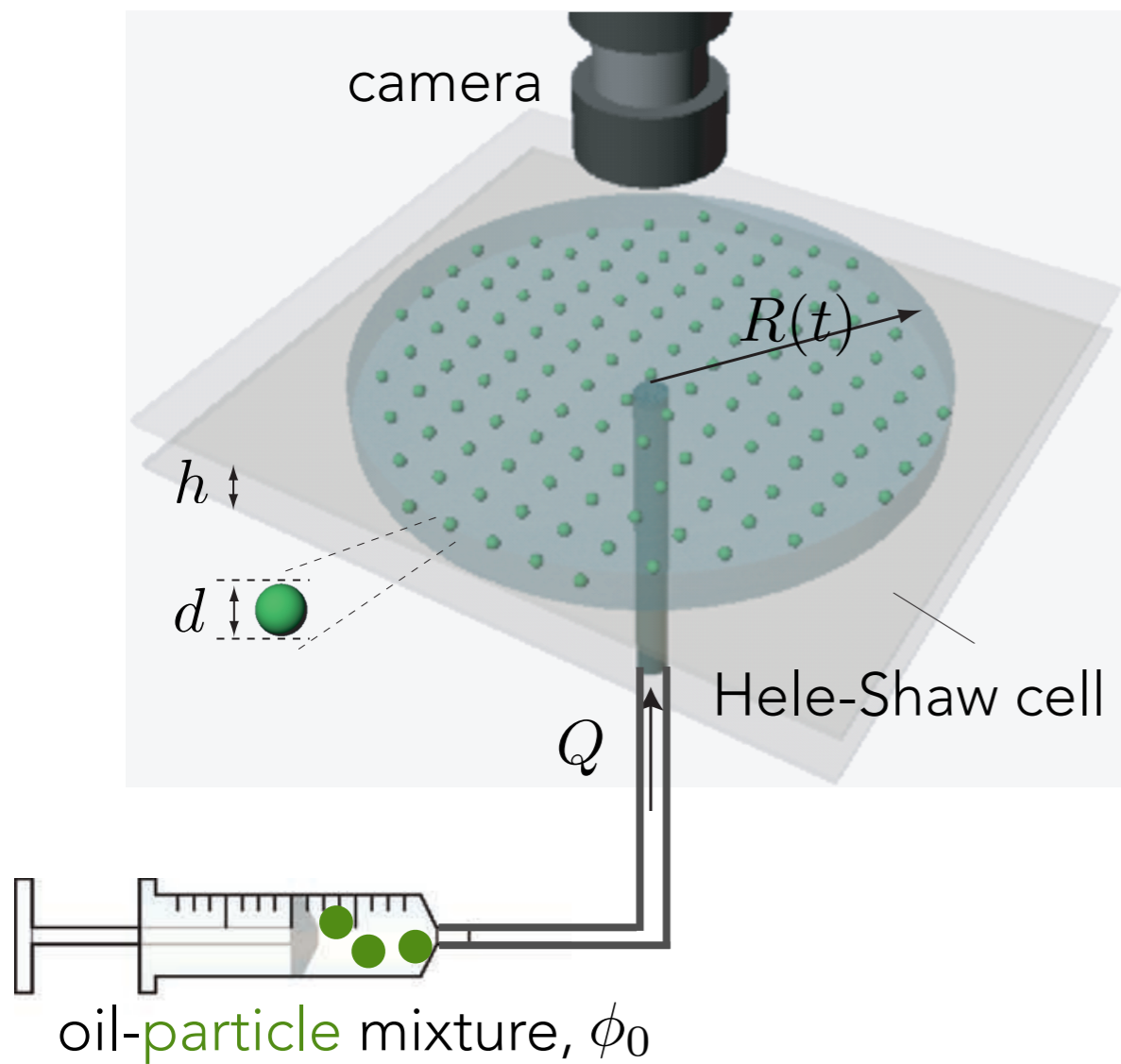
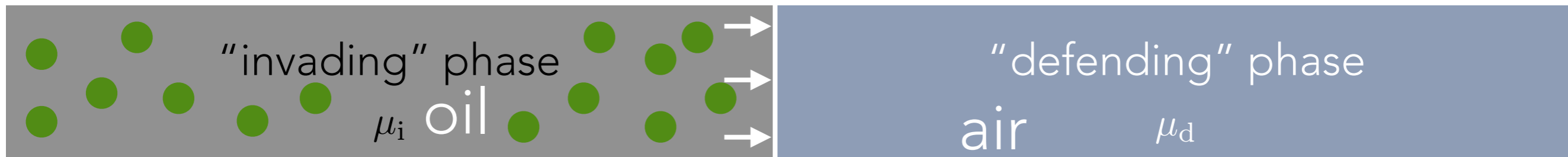


Praud & Swinney 2005

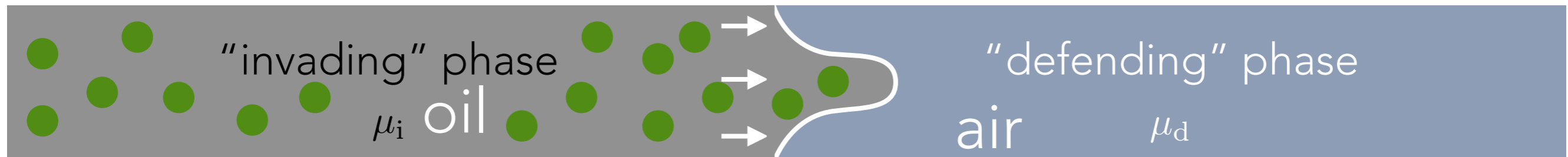


Pihler-Puzovic et al 2012

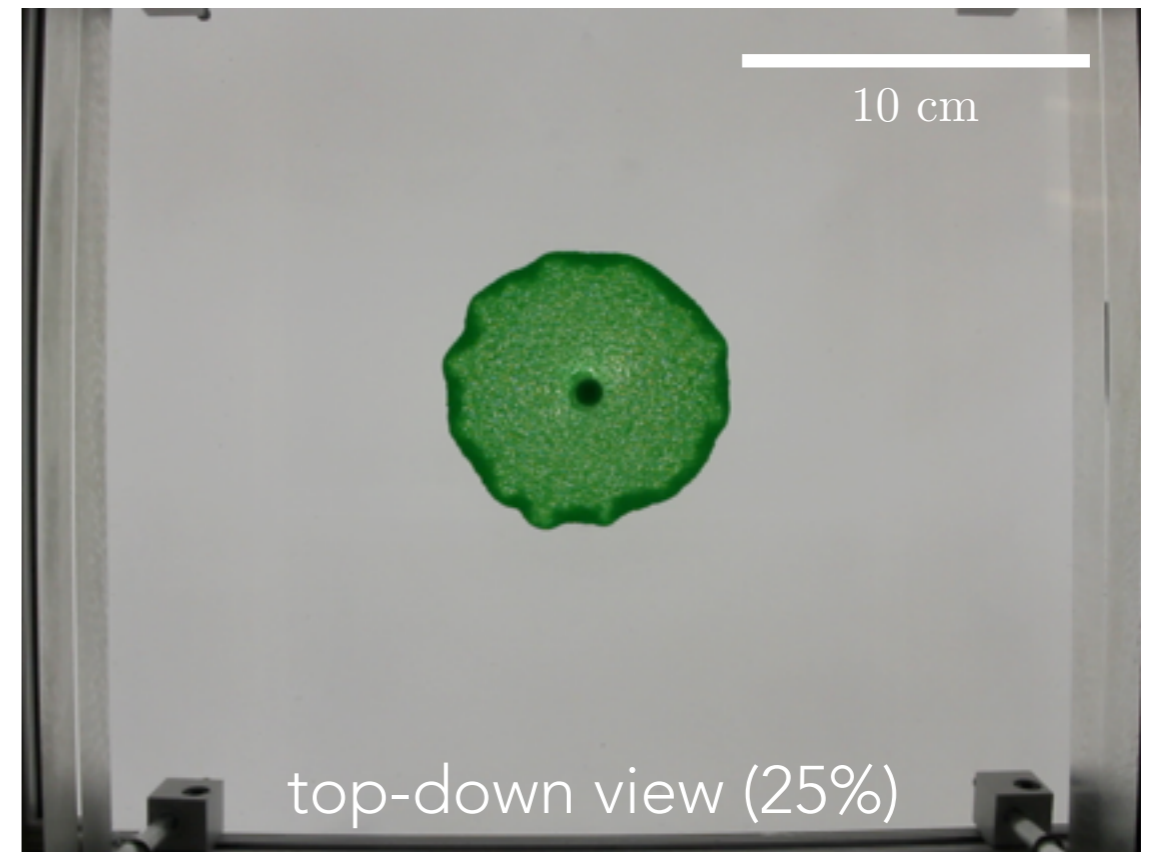
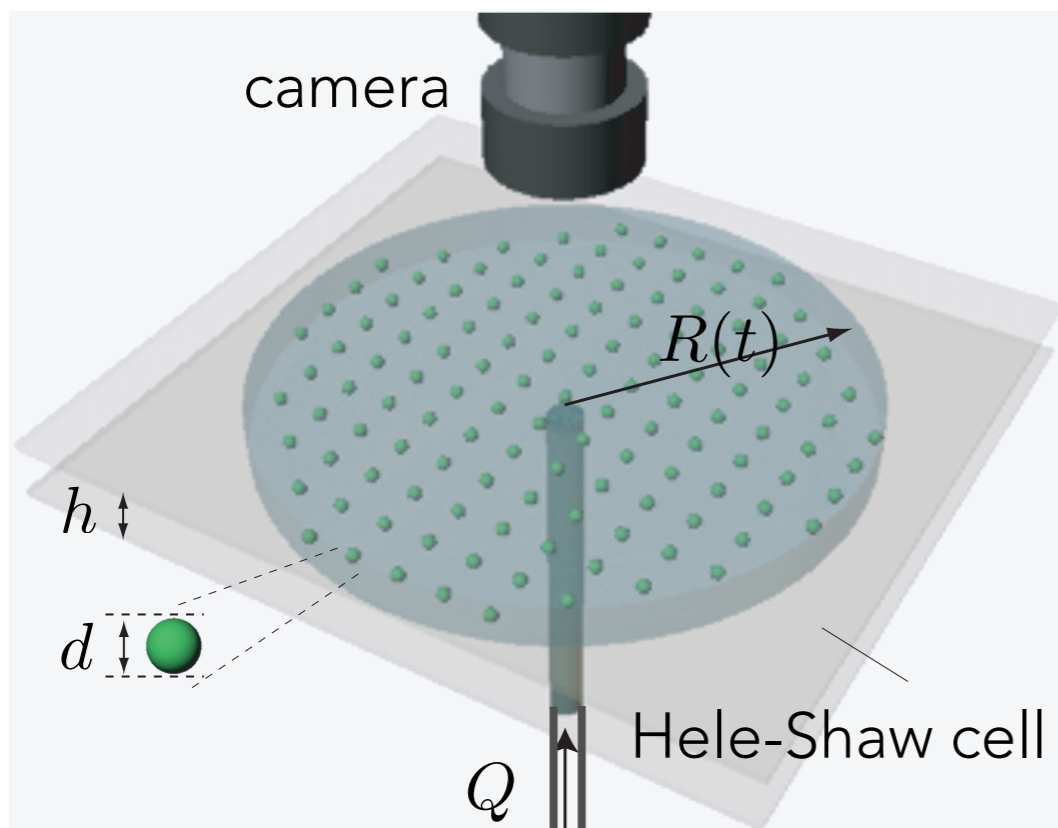
VISCOUS FINGERING + PARTICLES



VISCOUS FINGERING + PARTICLES

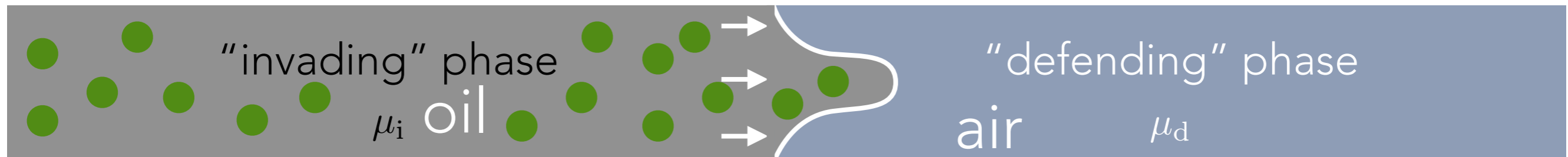


Particles **destabilize** the interface!

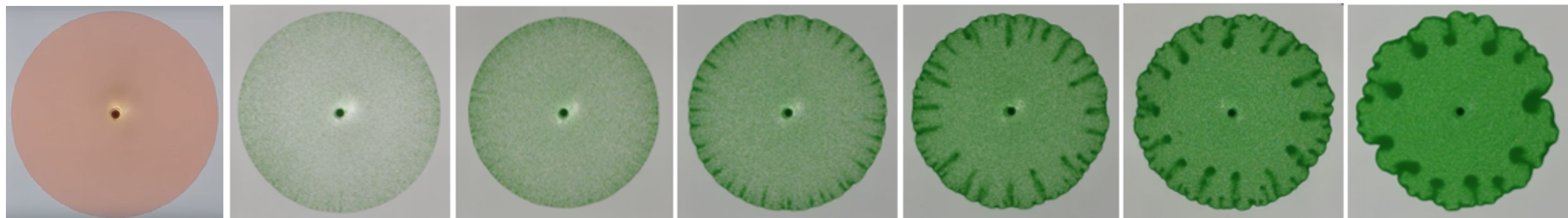
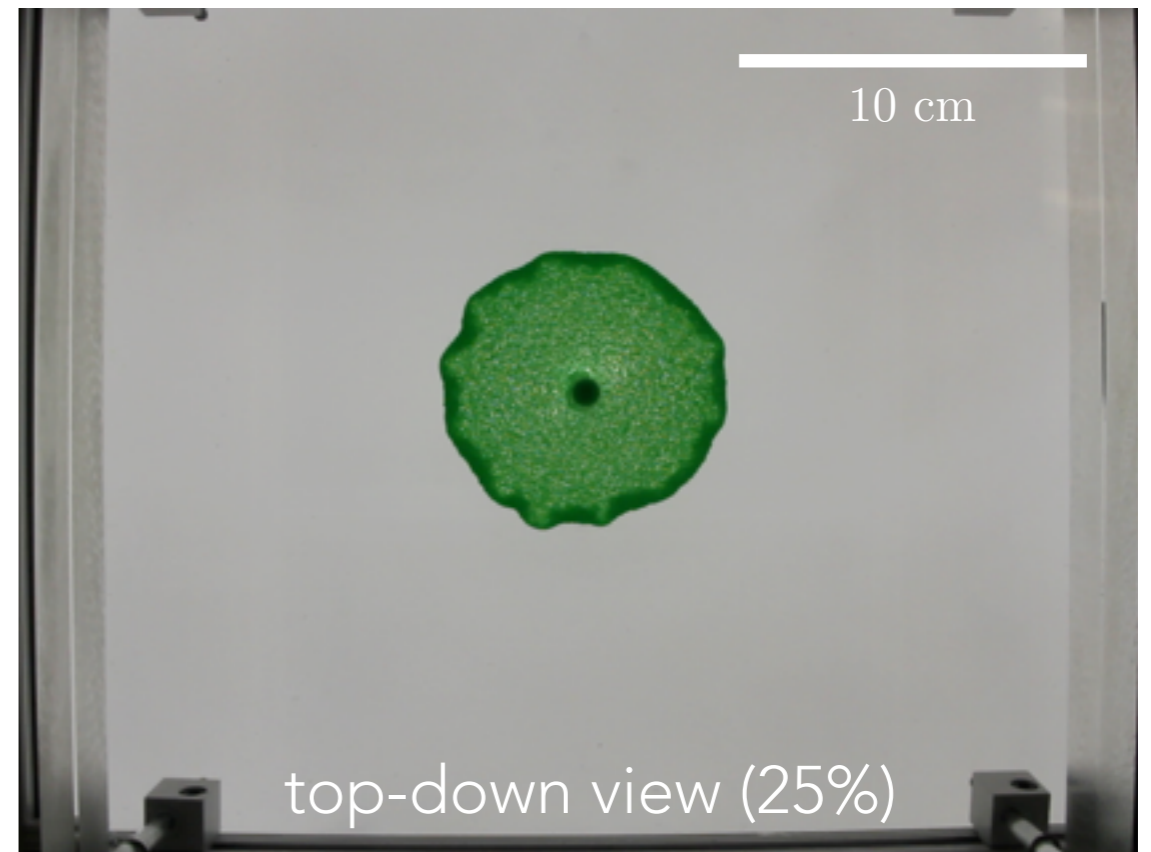
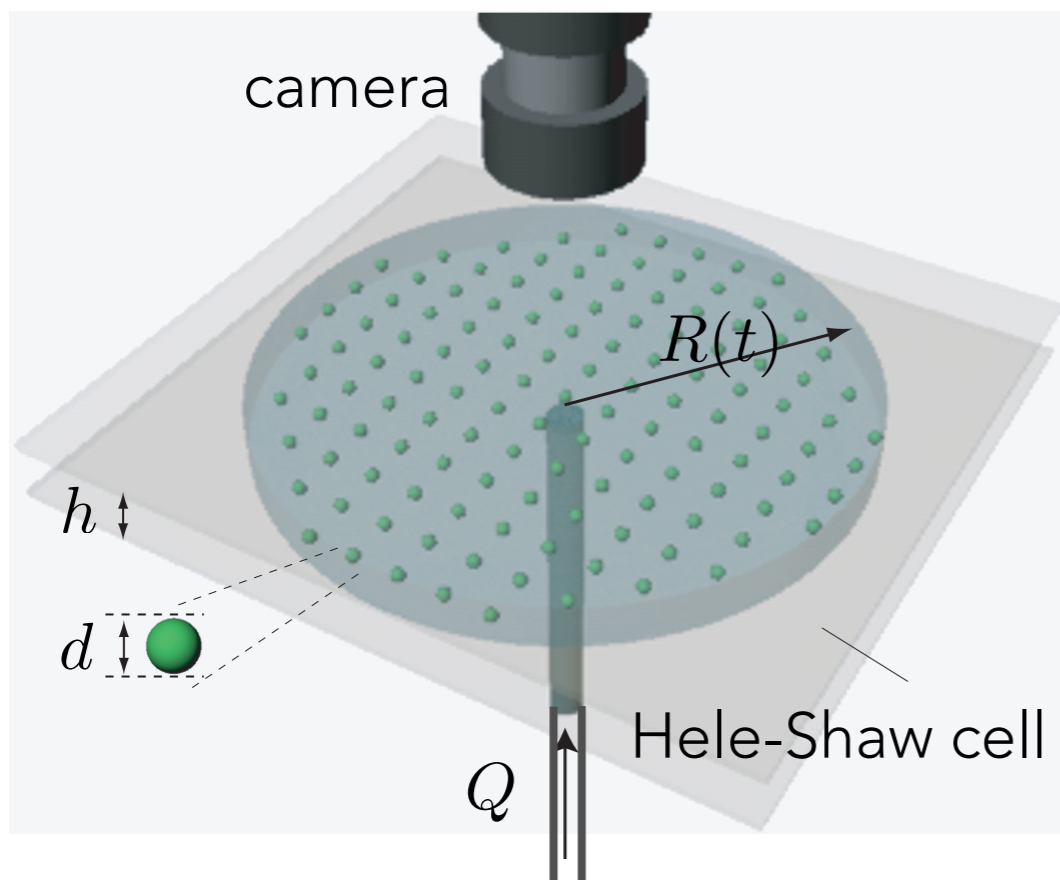


Tang et al 2000; Ramachandran & Leighton 2010

VISCOUS FINGERING + PARTICLES

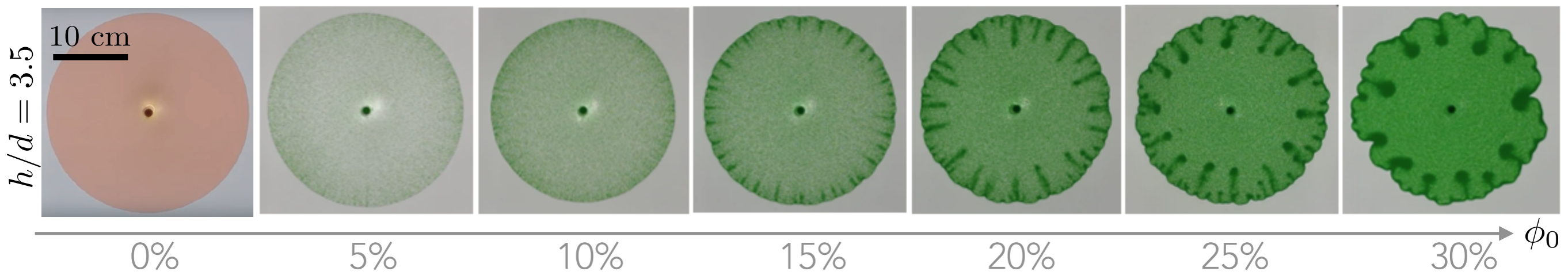
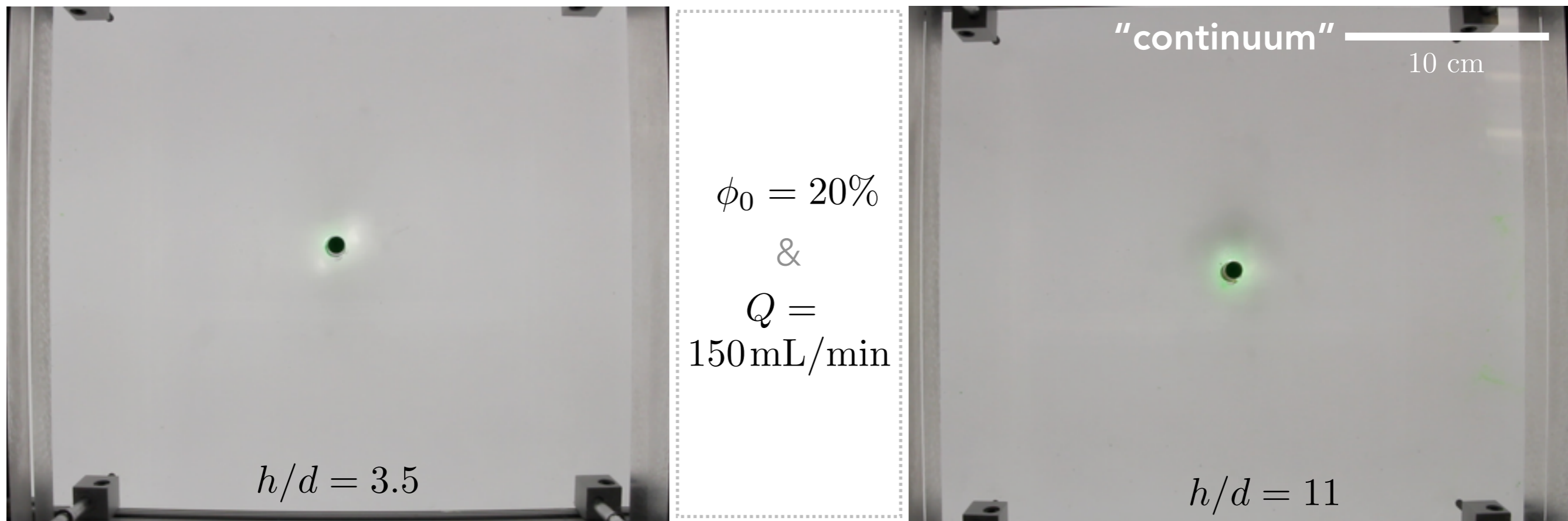


Particles **destabilize** the interface!

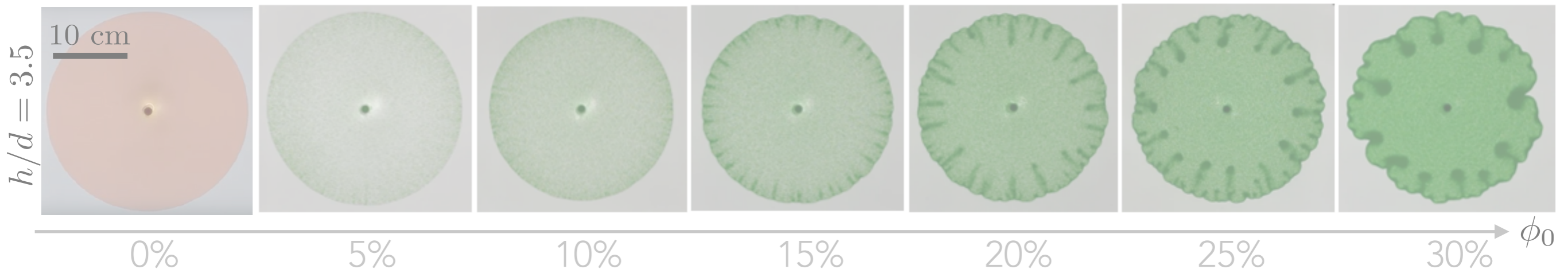
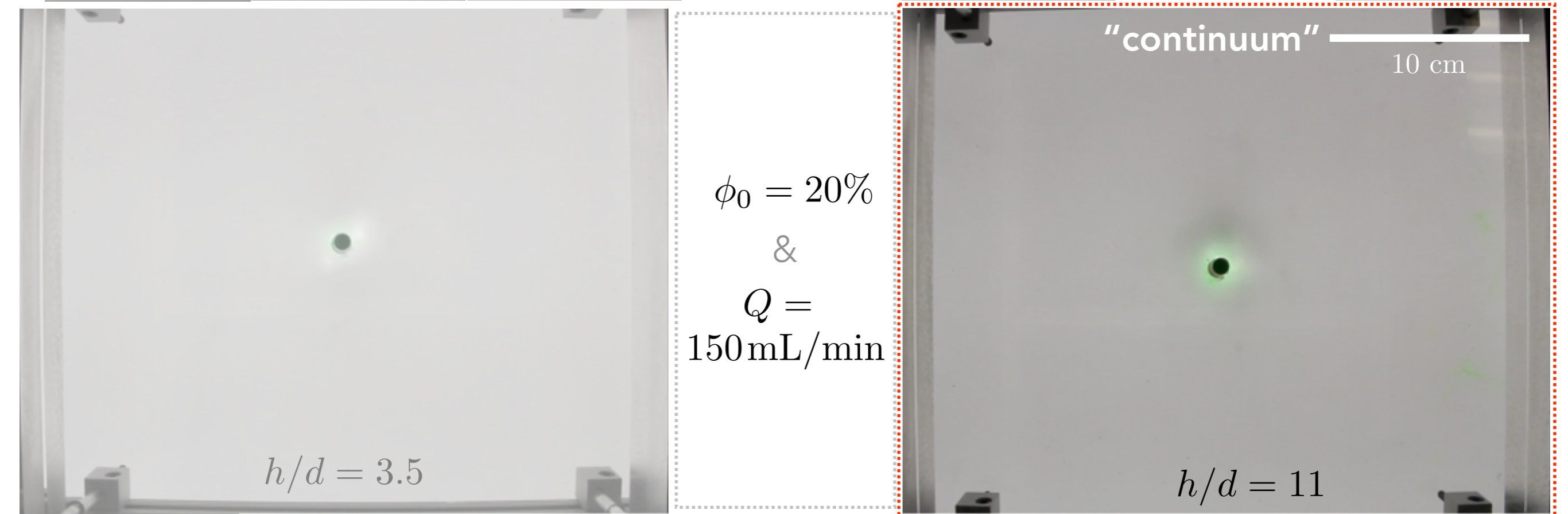
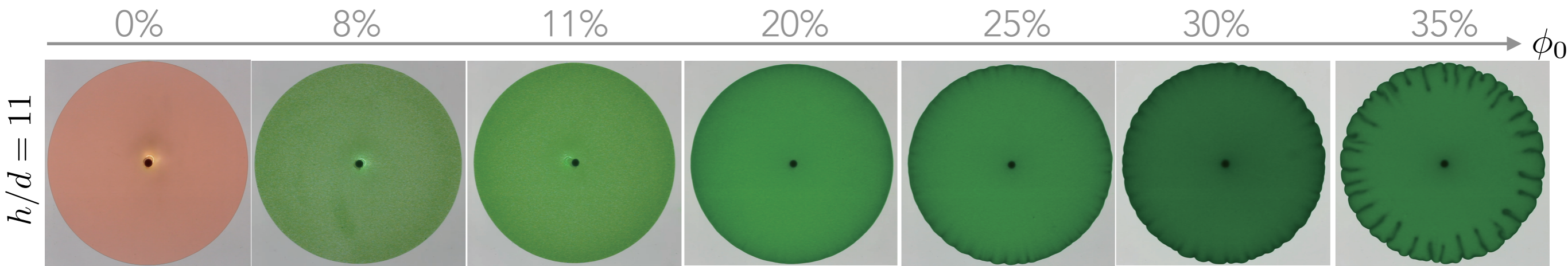


ϕ_0

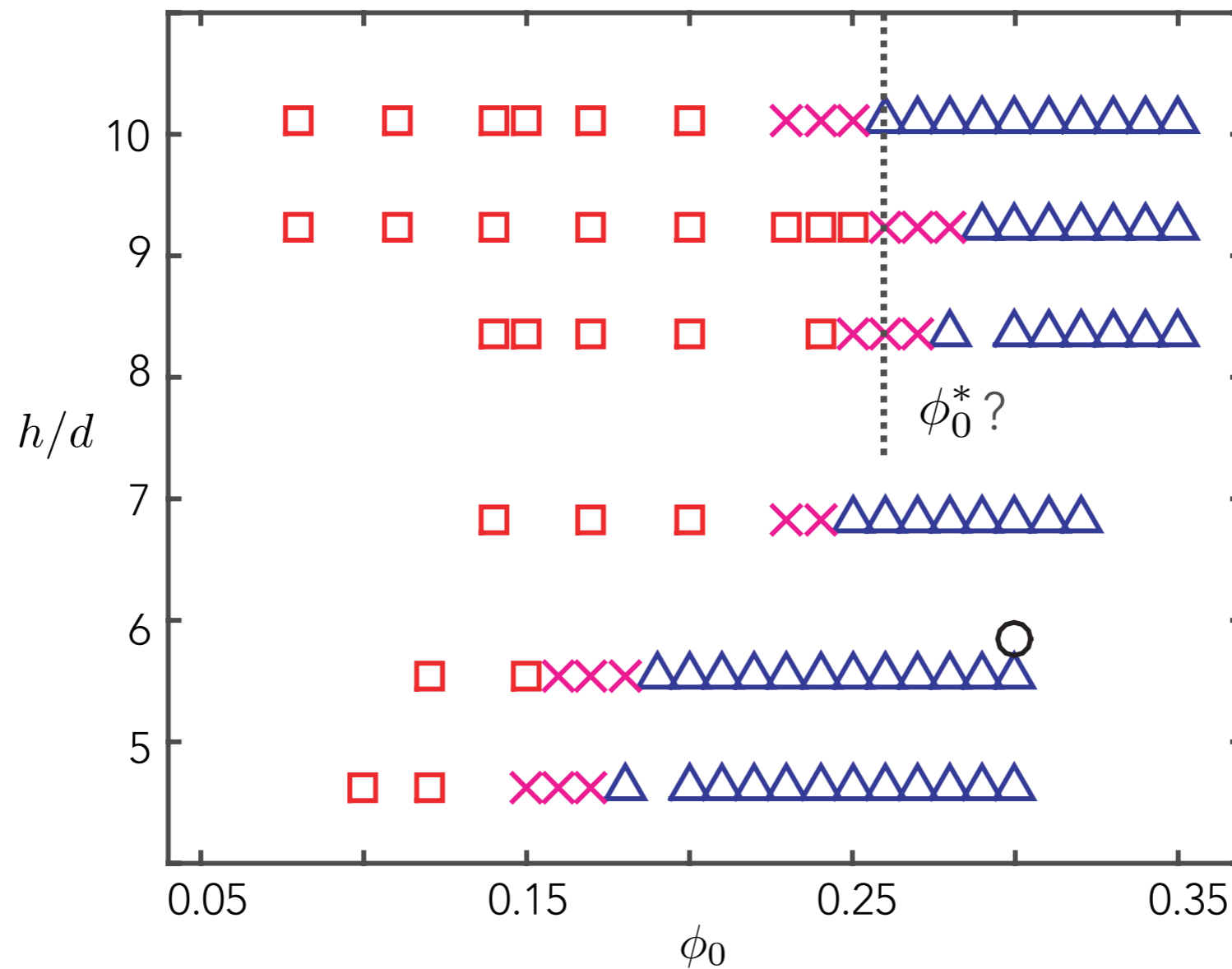
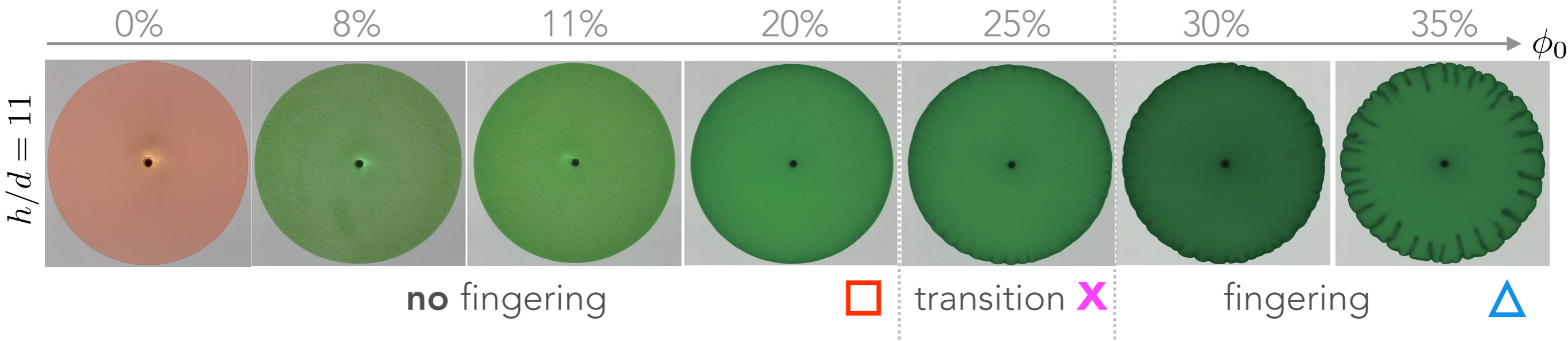
PARTICLE-INDUCED FINGERING



PARTICLE-INDUCED FINGERING

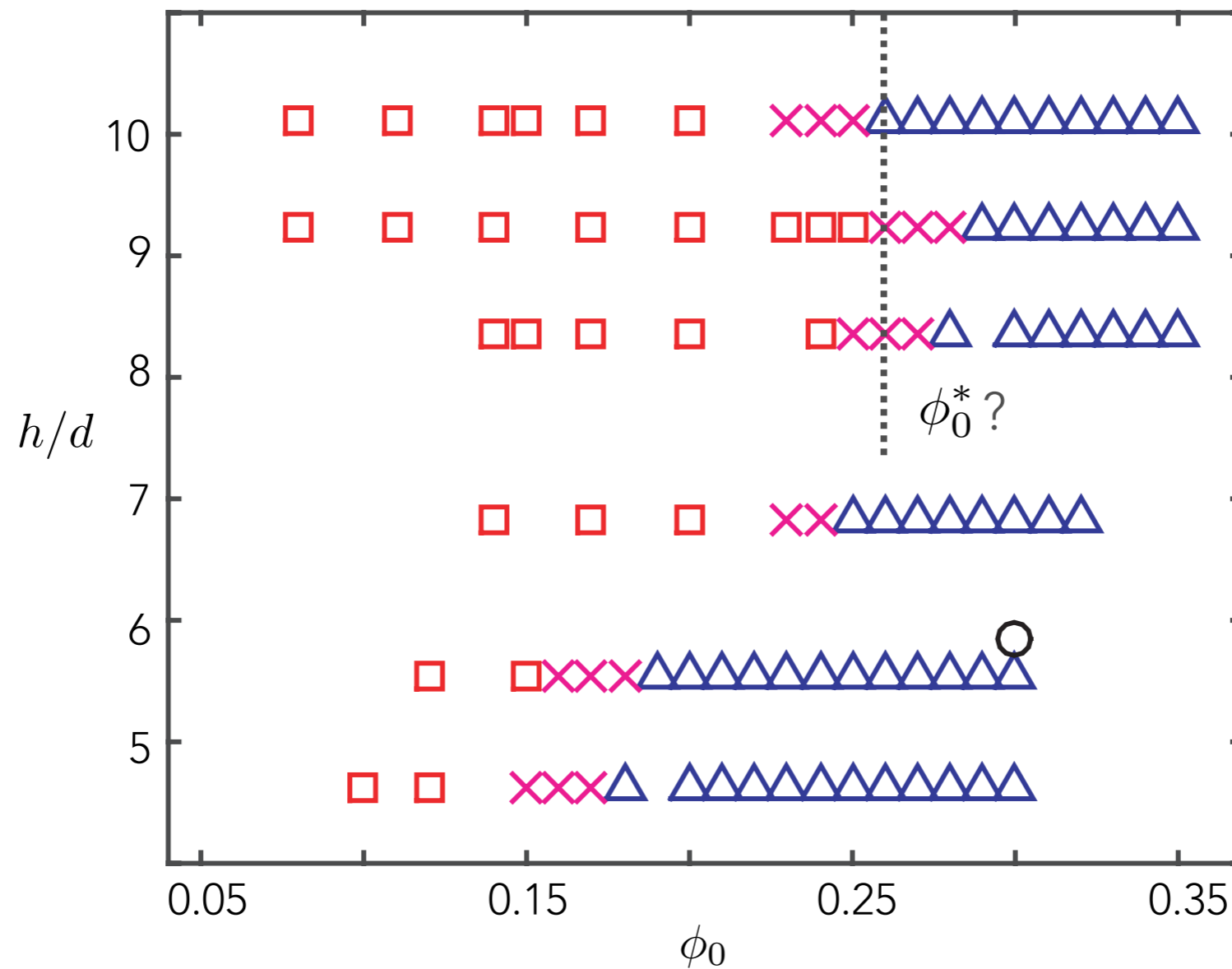
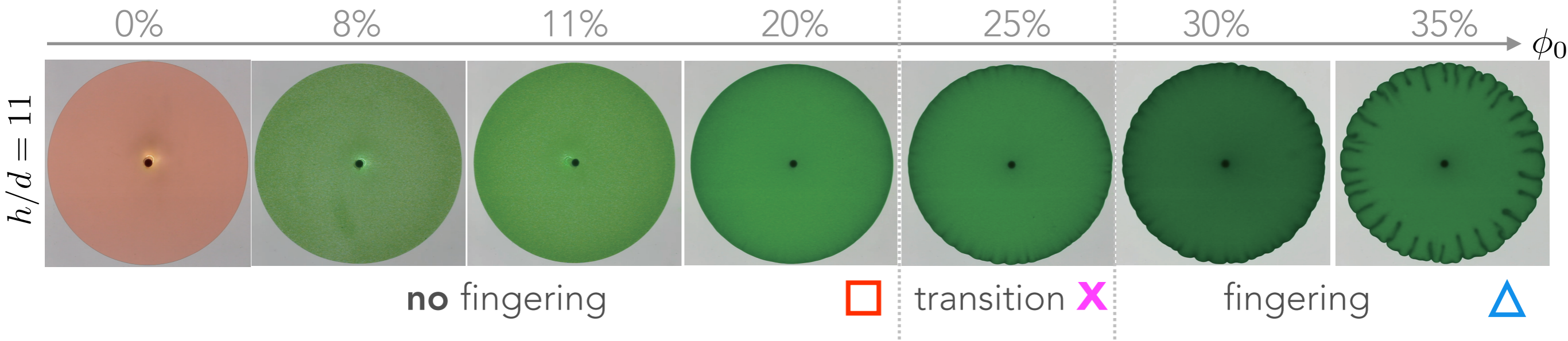


PARTICLE-INDUCED FINGERING



Eventually:
 What is the **critical particle concentration** in the continuum limit?

PARTICLE-INDUCED FINGERING



In this talk, we will focus on:

1. What is the **mechanism of fingering**?
2. Can we model the **particle-laden flow** upstream of the interface?

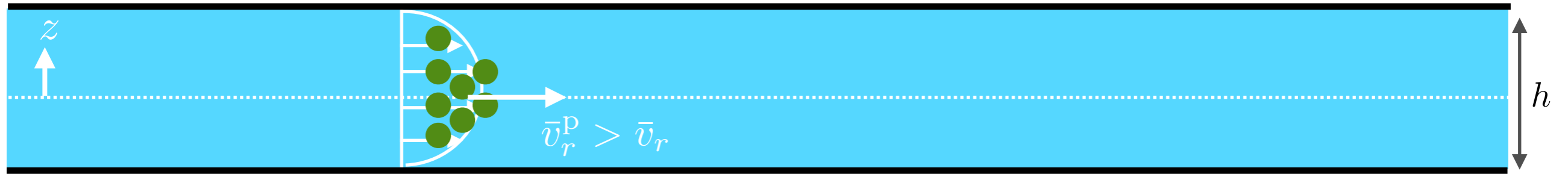
MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.



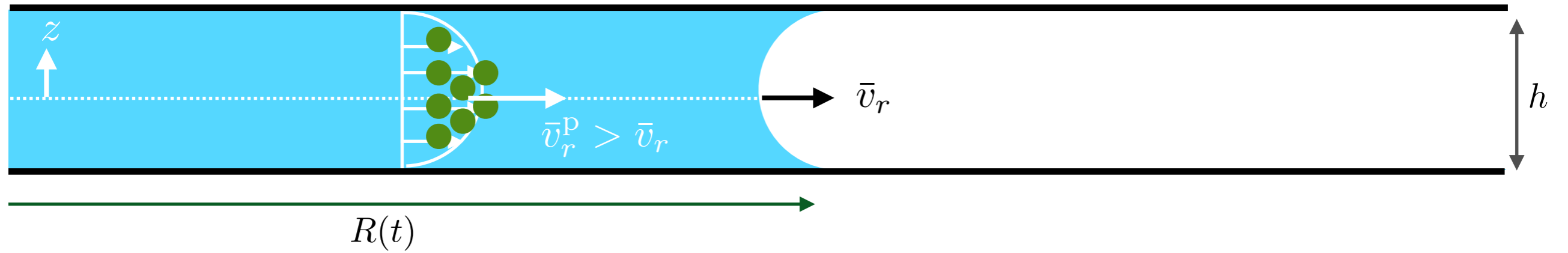
MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.



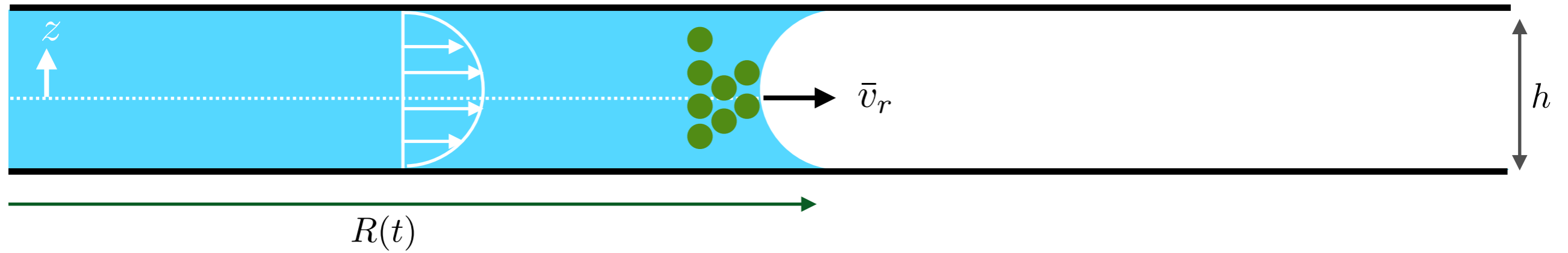
MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.



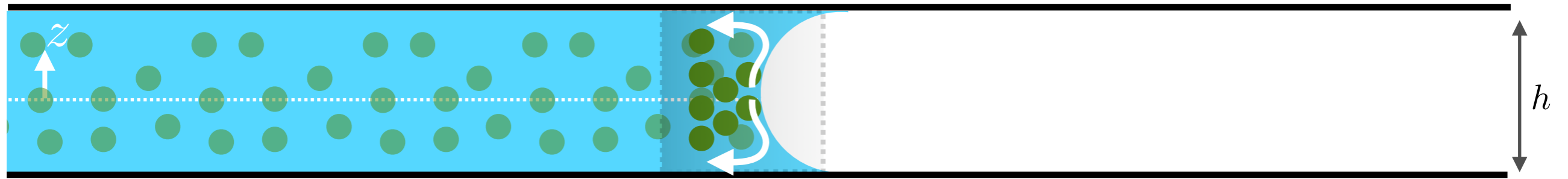
MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.



MECHANISM OF FINGERING

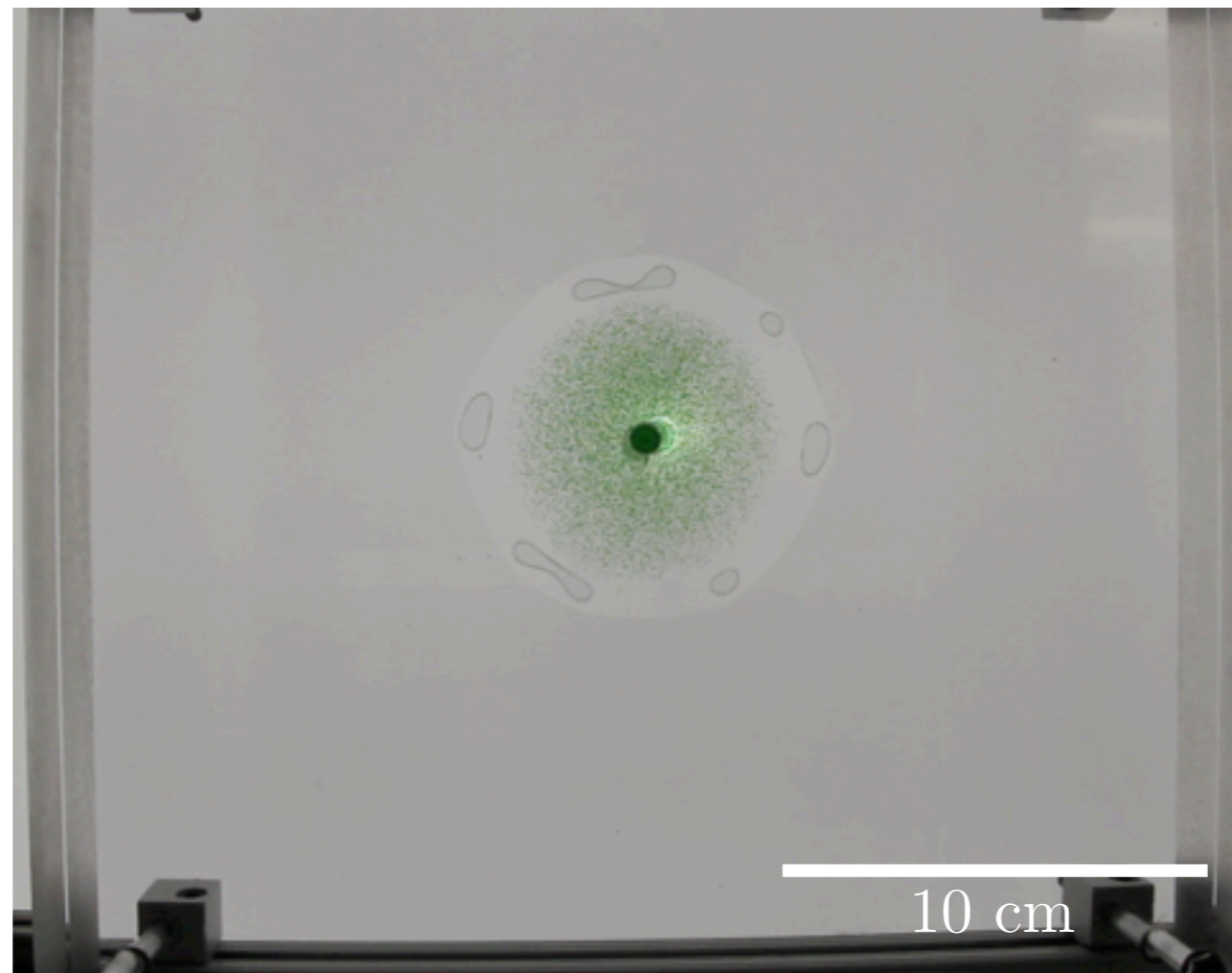
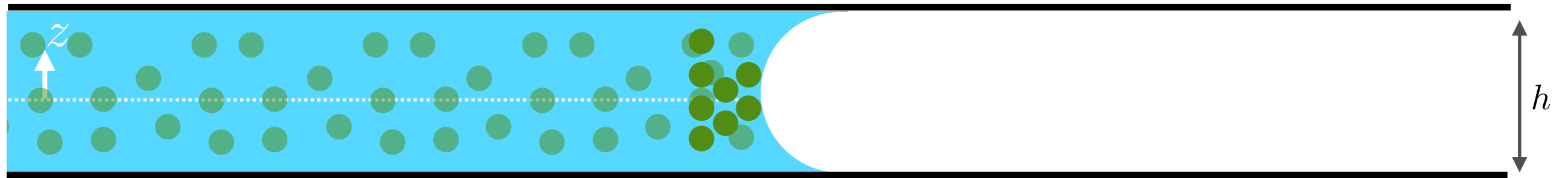
particle accumulation on the fluid-fluid interface.



"fountain flow" Coyle et al 1987; Karnis & Mason 1967

MECHANISM OF FINGERING

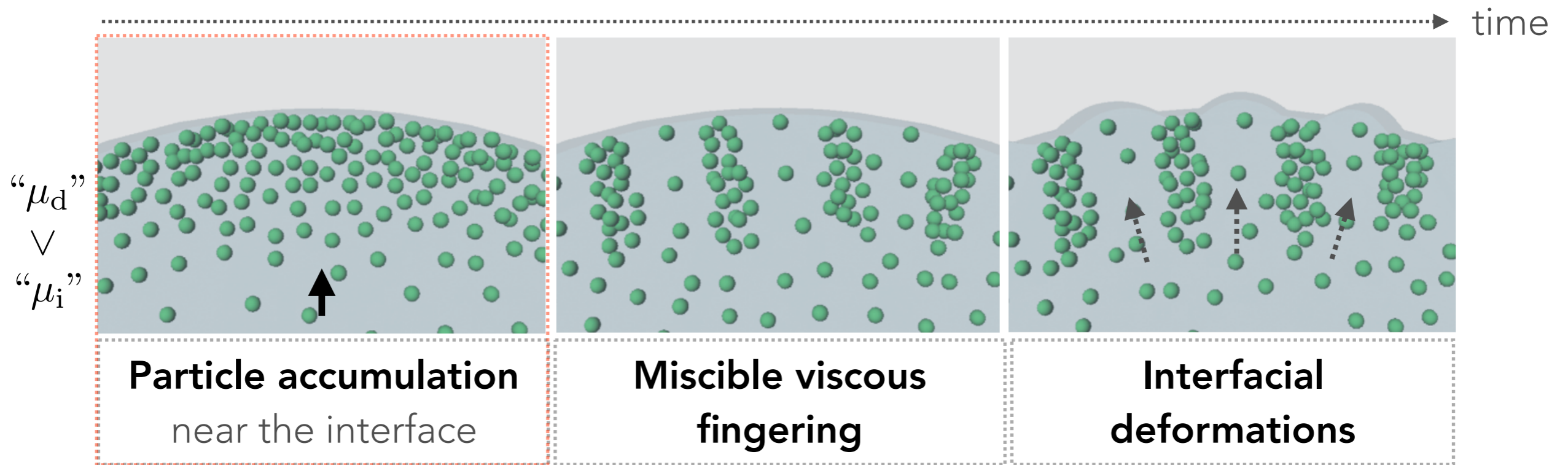
particle accumulation on the fluid-fluid interface.



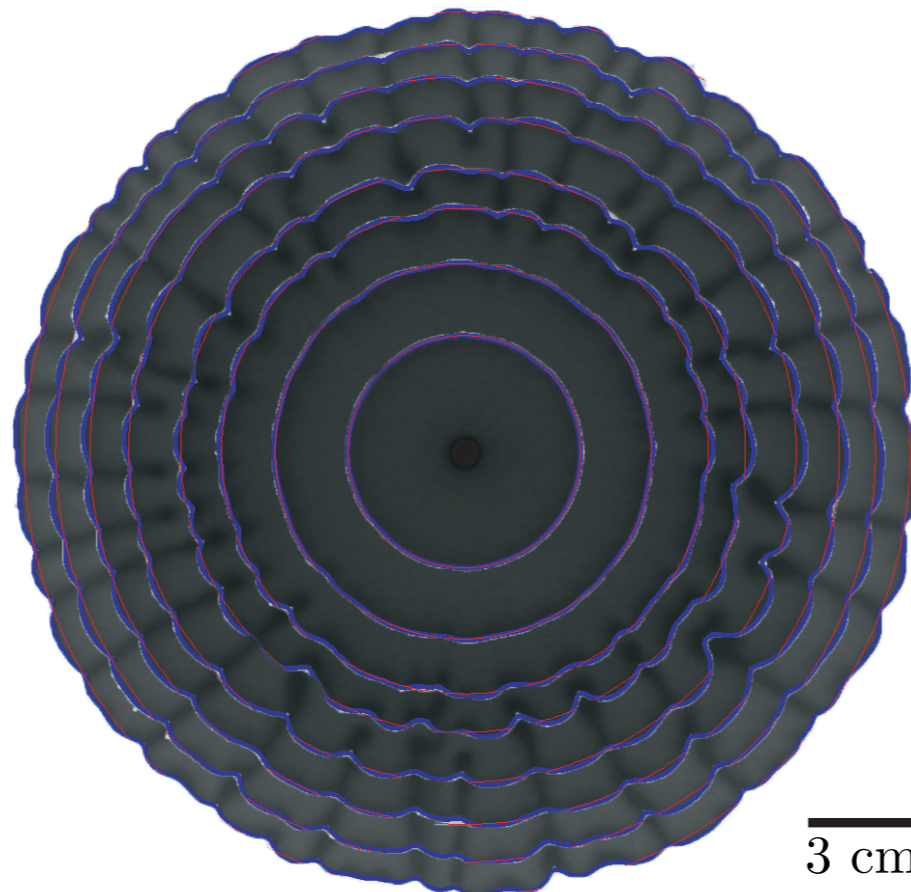
Tang et al 2000; Ramachandran & Leighton 2010, 2007 (particle accumulation on the meniscus in a tube)

MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.

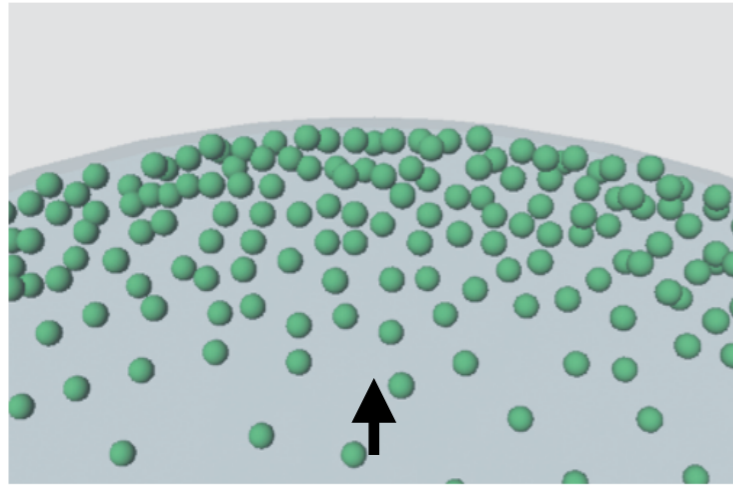


$$\phi_0 = 35\%$$

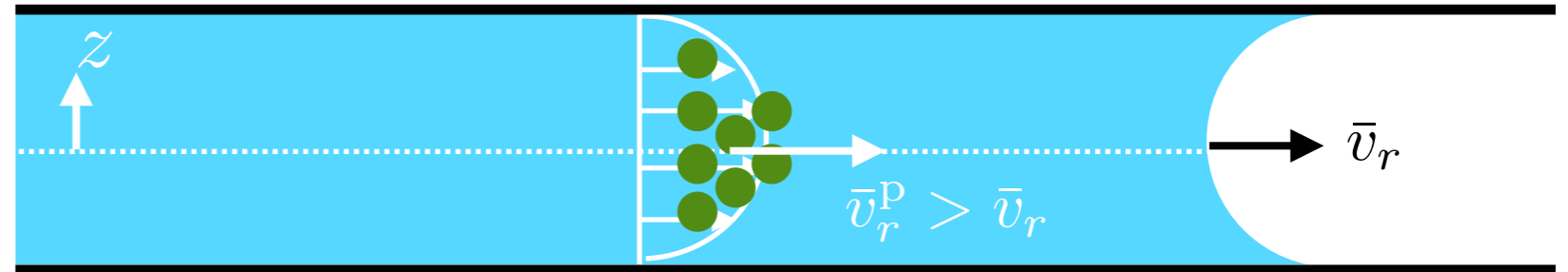


MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.



Particle accumulation
due to **shear-induced migration**

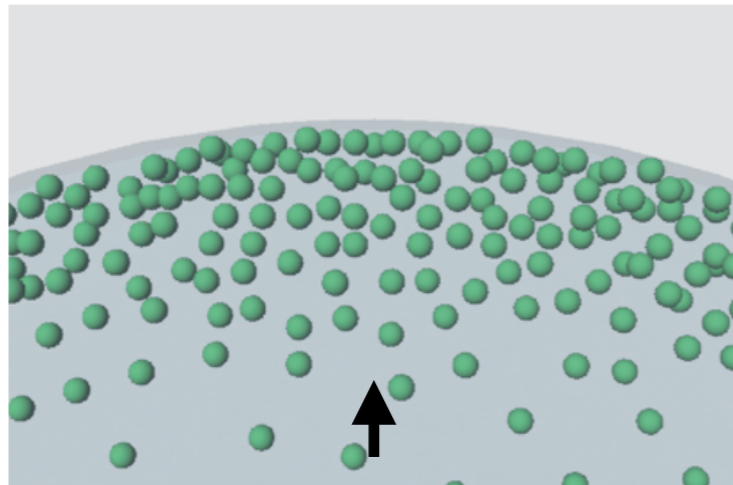


velocity ratio $\beta \equiv \frac{\bar{v}_r^p(r)}{\bar{v}_r(r)} > 1$ necessary condition for **accumulation**

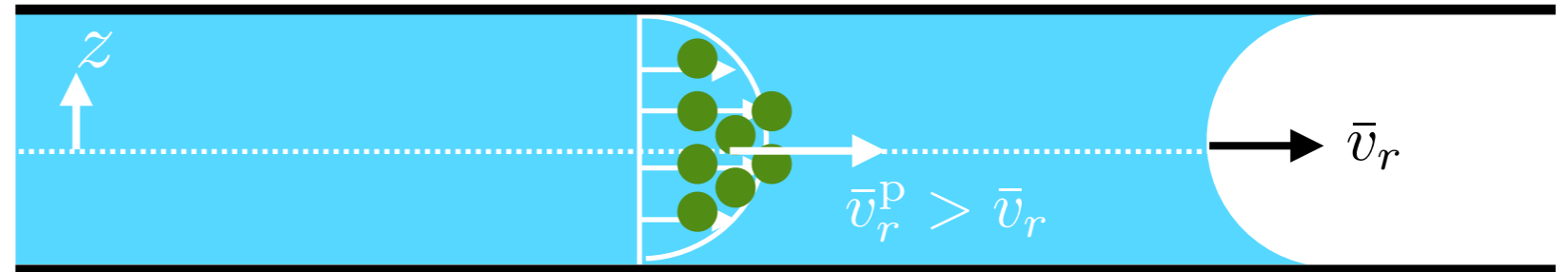
where $\bar{v}_r^p \equiv \frac{\int_{-h/2}^{h/2} v_r^p(r, z) \phi(r, z) dz}{\bar{\phi}(r)h}$ & $\bar{v}_r = \frac{Q}{2\pi r h}$

MECHANISM OF FINGERING

particle accumulation on the fluid-fluid interface.



Particle accumulation
due to **shear-induced migration**

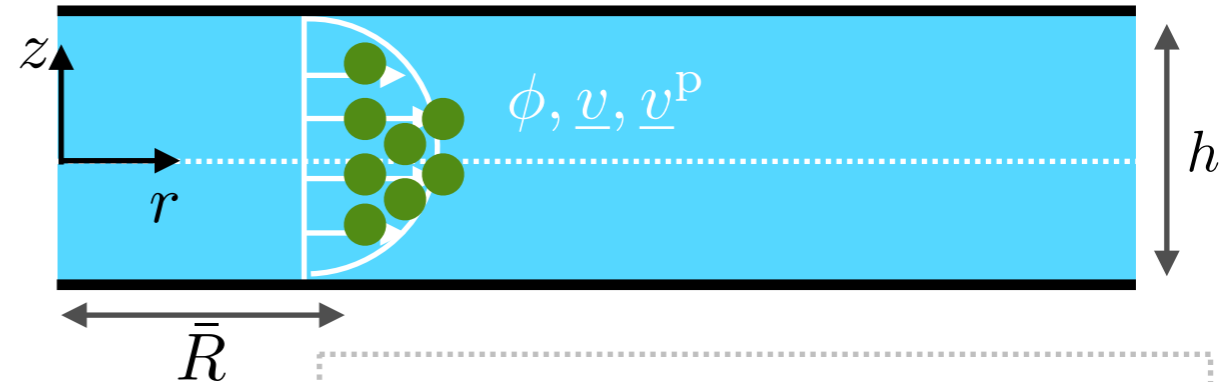


velocity ratio $\beta \equiv \frac{\bar{v}_r^P(r)}{\bar{v}_r(r)} > 1$ necessary condition for **fingering**

Calculate $\beta(\phi_0, h/d)$
by resolving the upstream flow field!

CONTINUUM MODEL

suspension balance approach Nott & Brady 1994



mixture mass conservation

$$\nabla \cdot \underline{v} = 0$$

mixture momentum

$$\nabla \cdot \underline{\underline{\Pi}} = 0$$

particulate mass conservation

$$\frac{\partial \phi}{\partial t} + \nabla \cdot (\phi \underline{v}^p) = 0$$

particulate momentum

$$\nabla \cdot \underline{\underline{\Pi}}^p - \frac{18\mu_1}{d^2} \frac{\phi}{f(\phi)} (\underline{v}^p - \underline{v}) = 0$$

Lubrication approximations:

$$h/\bar{R} \ll 1$$

$$\underline{v} = \frac{F(z)}{r} \underline{e}_r, \quad \frac{\partial}{\partial \theta} = 0$$

(axisymmetric)

kinematic relationship

$$\underline{v} = \phi \underline{v}^p + (1 - \phi) \underline{v}^f$$

constitutive relationships

$$\underline{\underline{\Pi}} = -p \underline{\underline{I}} + \mu_1 (\nabla \underline{v} + \nabla \underline{v}^T) + \underline{\underline{\Pi}}^p$$

$$\underline{\underline{\Pi}}^p = \underline{\underline{\Pi}}_n^p(\dot{\gamma}, \mu_n(\phi)) + (\mu_s(\phi) - \mu_1) (\nabla \underline{v} + \nabla \underline{v}^T)$$

particulate normal stress
 $\sim \mu_1 \nabla \dot{\gamma}$

empirical relationships

$$\mu_s \approx \mu_1 \frac{e^{-2.34\phi}}{(1 - \phi/\phi_m)^3}$$

Zarraga et al 2000

CONTINUUM MODEL

suspension balance approach + **lubrication** approximations

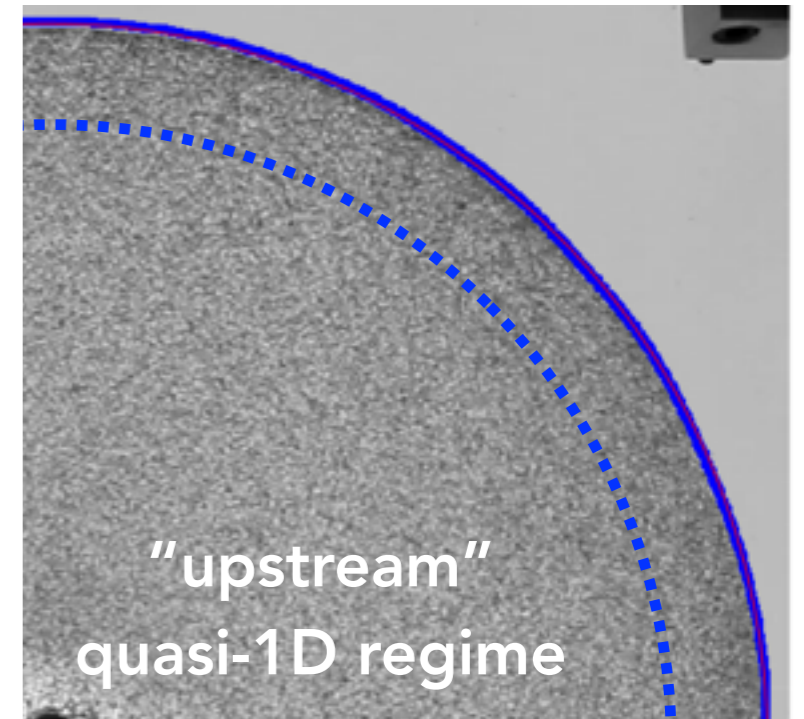
- mixture momentum
- particulate mass + momentum
- constant mixture flux
- constant particulate flux

$$r^* \frac{dp^*}{dr^*} (z^* - 1/2) = \frac{\mu_s(\phi)}{\mu_l} \frac{dF^*}{dz^*}$$

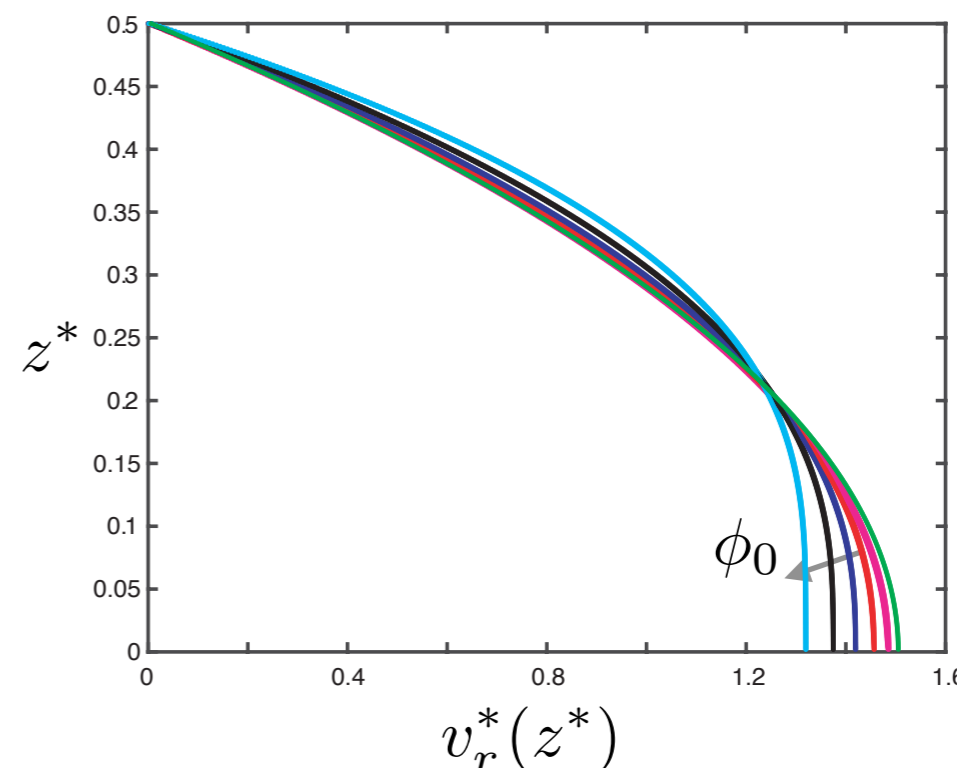
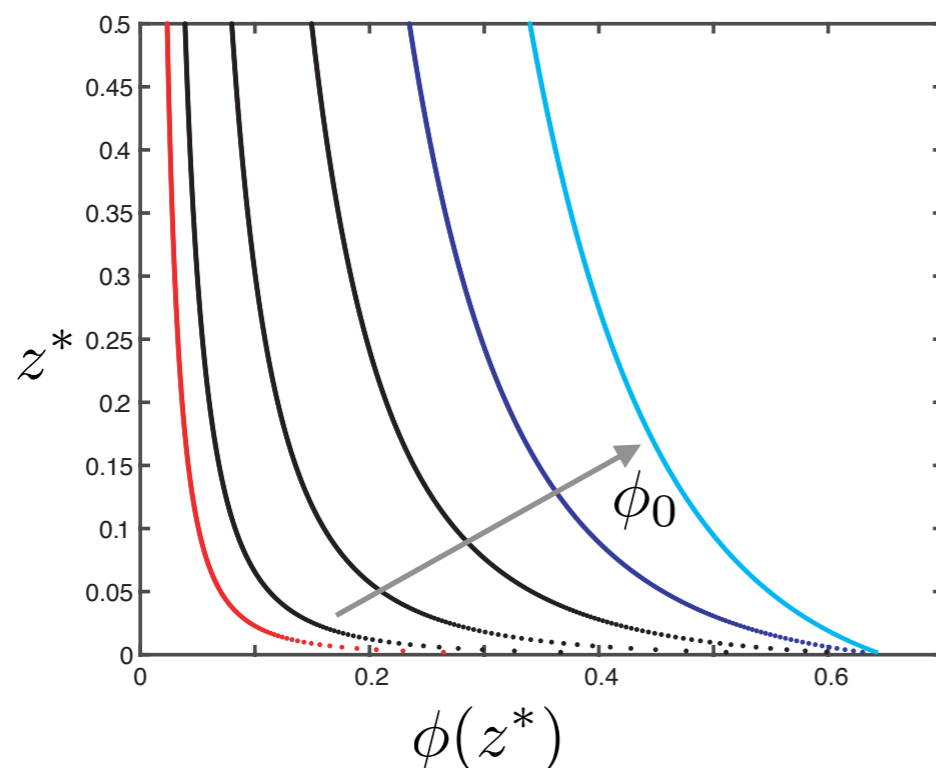
$$\text{const} = \frac{\mu_n(\phi)}{\mu_l} \frac{dF^*}{dz^*}$$

$$\frac{1}{2} = \int_0^{1/2} F^*(z^*) dz^*$$

$$\frac{\phi_0}{2} = r^* \int_0^{1/2} \phi(z) v_r^{P*} dz^*$$



$\phi = \phi(z)$ only



CONTINUUM MODEL

suspension balance approach + **lubrication** approximations

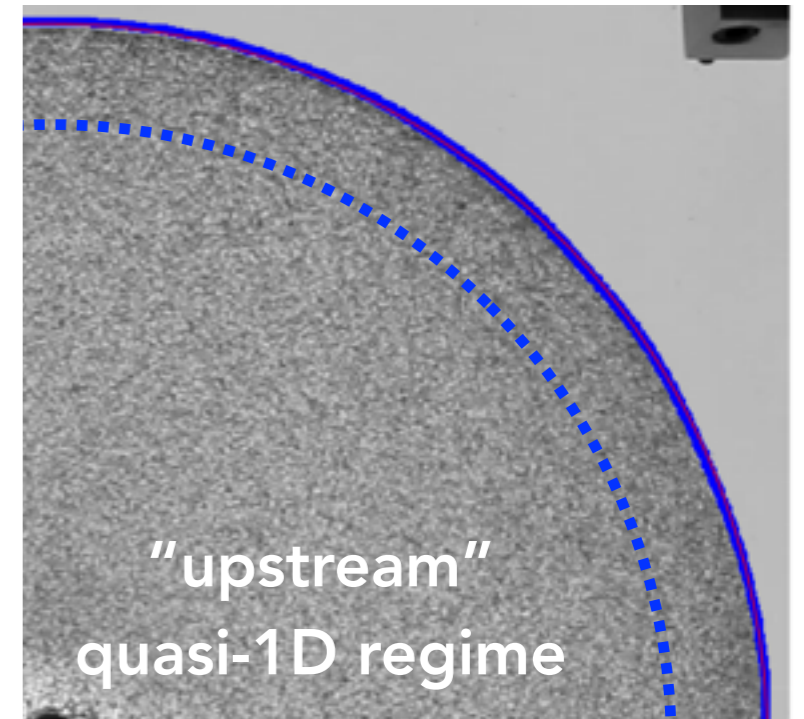
mixture momentum
particulate mass + momentum
constant mixture flux
constant particulate flux

$$r^* \frac{dp^*}{dr^*} (z^* - 1/2) = \frac{\mu_s(\phi)}{\mu_l} \frac{dF^*}{dz^*}$$

$$\text{const} = \frac{\mu_n(\phi)}{\mu_l} \frac{dF^*}{dz^*}$$

$$\frac{1}{2} = \int_0^{1/2} F^*(z^*) dz^*$$

$$\frac{\phi_0}{2} = r^* \int_0^{1/2} \phi(z) v_r^{\text{P}*} dz^*$$

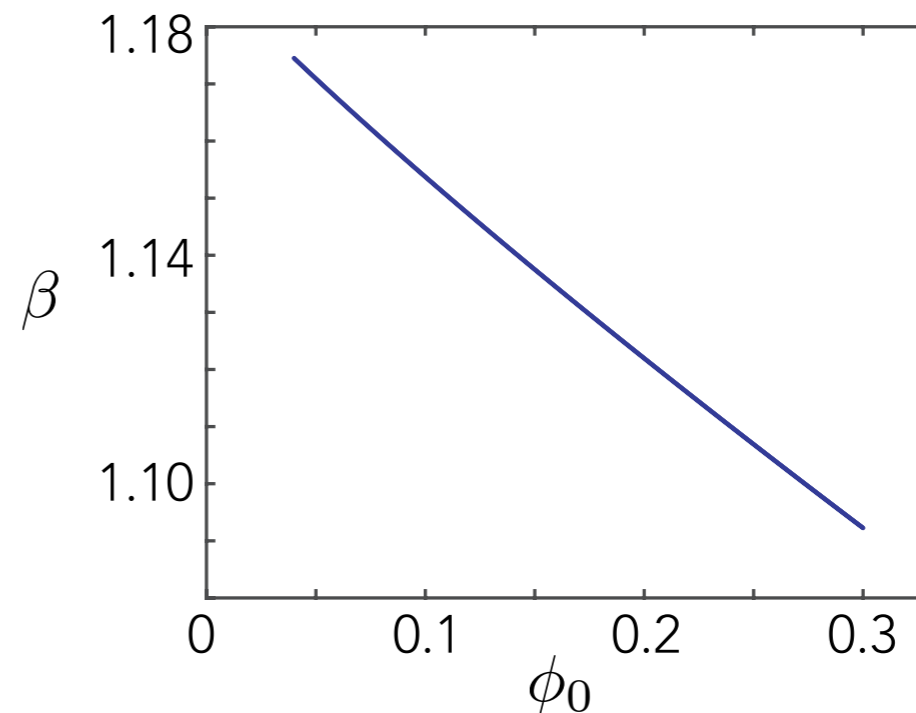


$\phi = \phi(z)$ only

velocity ratio

$$\beta = \frac{\int_{-h/2}^{h/2} v_r^{\text{P}}(r, z) \phi(r, z) dz}{\bar{\phi}(r) \bar{v}_r(r) h} > 1$$

necessary condition for **fingering**



CONTINUUM MODEL

suspension balance approach + lubrication approximations

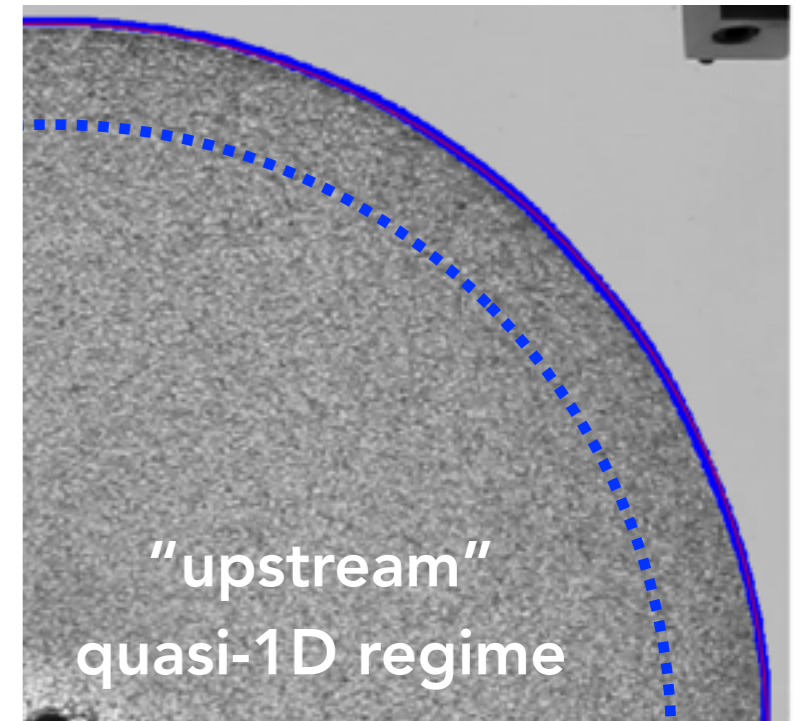
mixture momentum
particulate mass + momentum
constant mixture flux
constant particulate flux

$$r^* \frac{dp^*}{dr^*} (z^* - 1/2) = \frac{\mu_s(\phi)}{\mu_l} \frac{dF^*}{dz^*}$$

$$\text{const} = \frac{\mu_n(\phi)}{\mu_l} \frac{dF^*}{dz^*}$$

$$\frac{1}{2} = \int_0^{1/2} F^*(z^*) dz^*$$

$$\frac{\phi_0}{2} = r^* \int_0^{1/2} \phi(z) v_r^{p*} dz^*$$

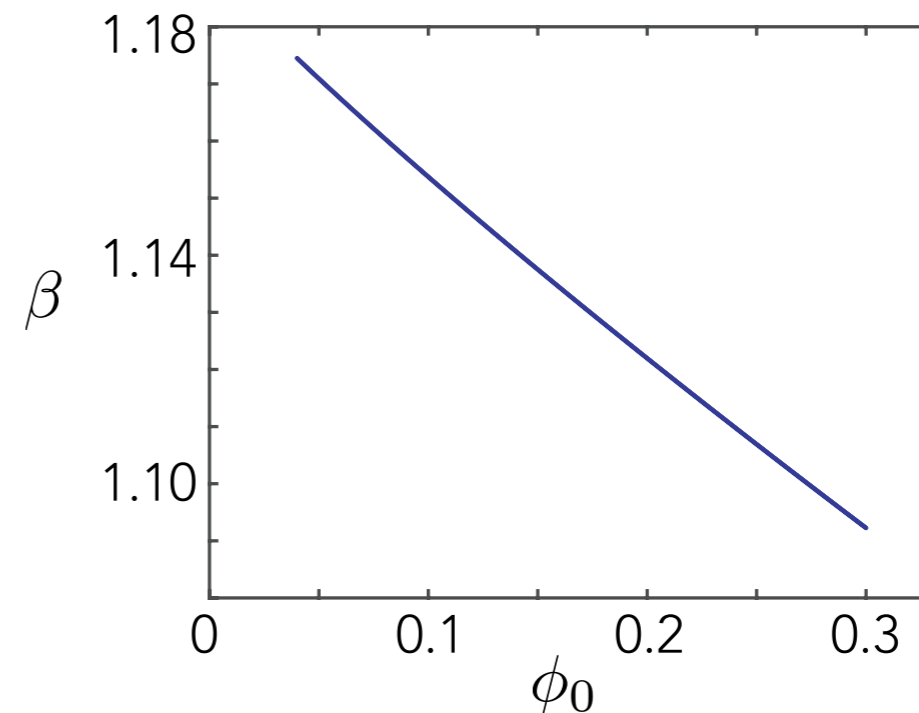


$\phi = \phi(z)$ only

velocity ratio

$$\beta = \frac{\int_{-h/2}^{h/2} v_r^p(r, z) \phi(r, z) dz}{\bar{\phi}(r) \bar{v}_r(r) h} > 1$$

Can we validate the velocity ratio experimentally?



MODEL VALIDATION:

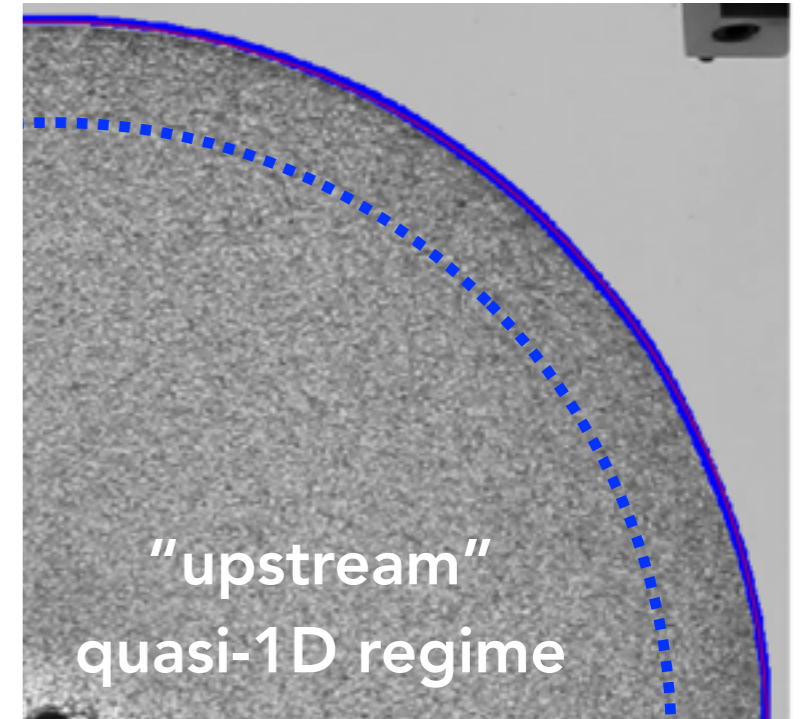
from **accumulation** to **fingering**

mass conservation
in upstream
regime

$$\phi_0 Q = 2\pi r \int_{-h/2}^{h/2} v_r^p(z) \phi(z) dz$$

$$\beta = \phi_0 / \bar{\phi}_{\text{up}}$$

measure experimentally



$$\bar{\phi}_{\text{up}} = \frac{1}{h} \int_{-h/2}^{h/2} \phi(z) dz$$

MODEL VALIDATION:

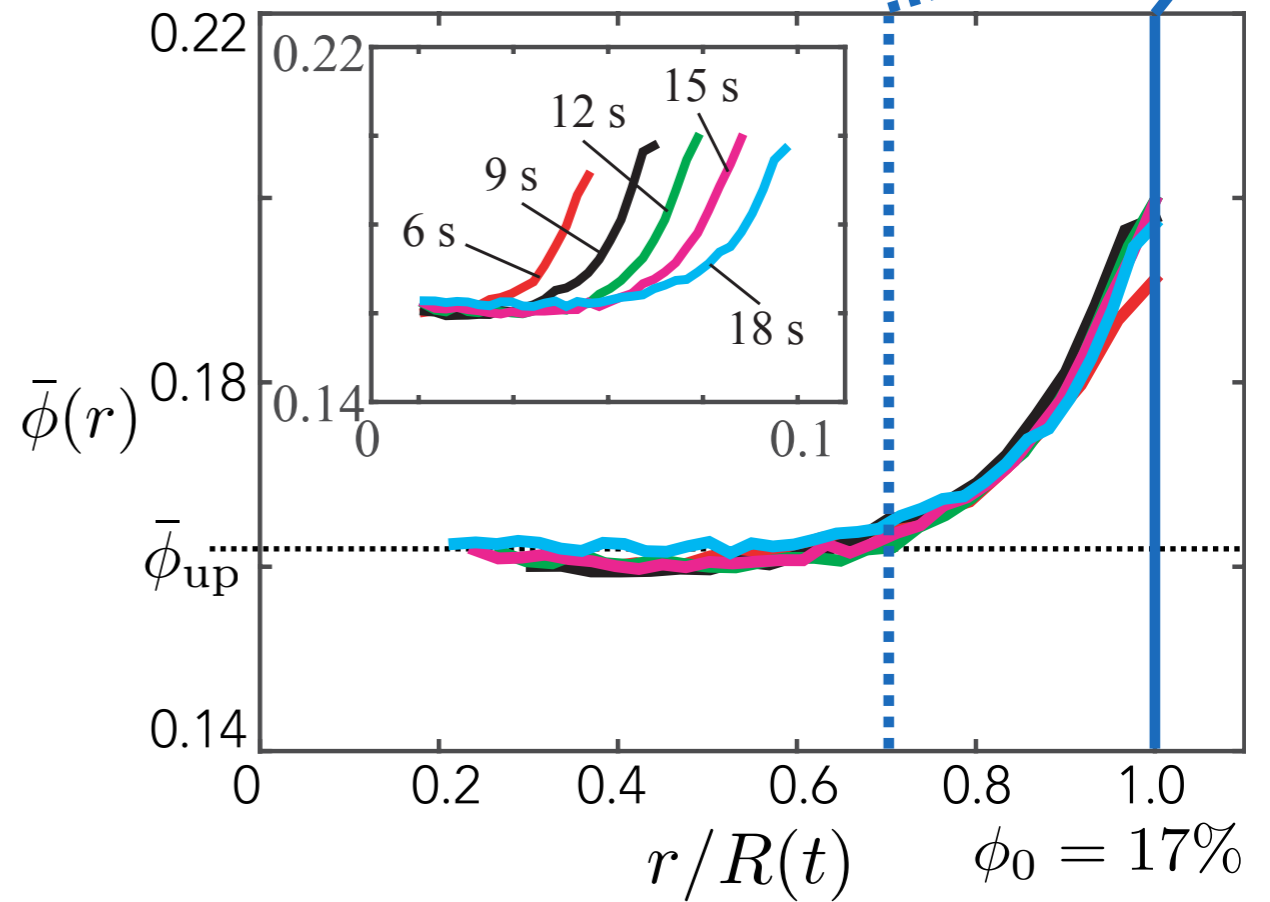
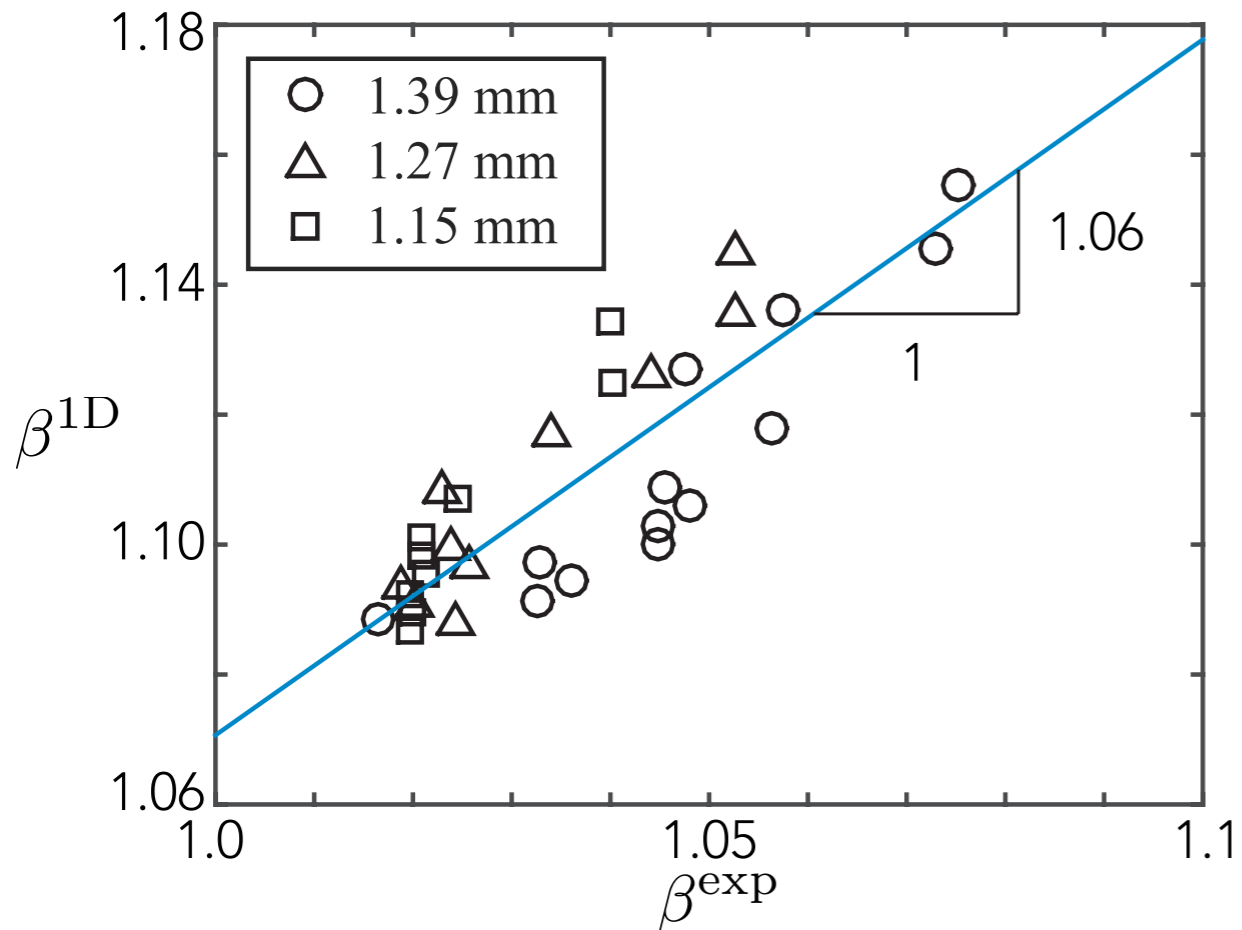
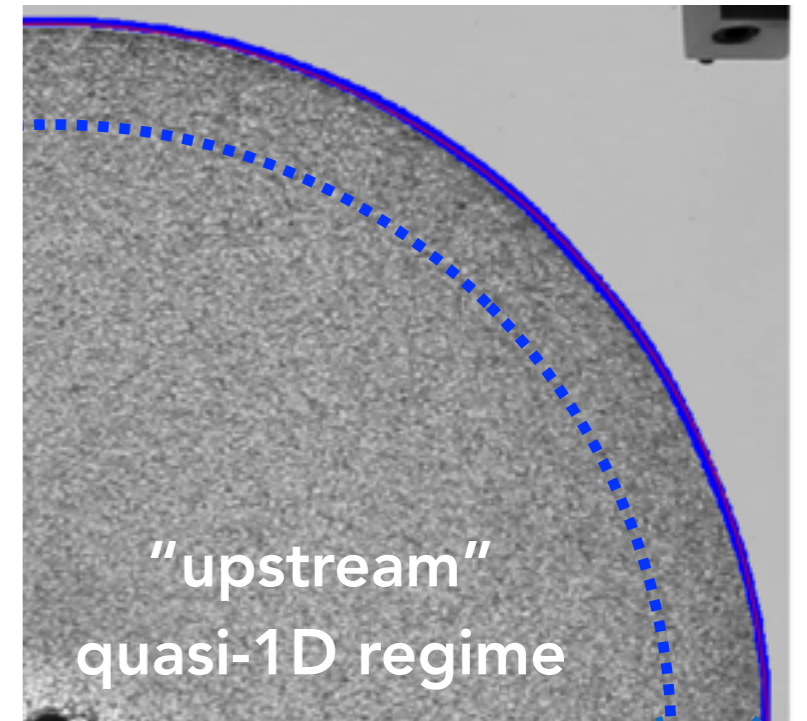
from **accumulation** to **fingering**

mass conservation
in upstream
regime

$$\phi_0 Q = 2\pi r \int_{-h/2}^{h/2} v_r^p(z) \phi(z) dz$$

$$\beta = \phi_0 / \bar{\phi}_{\text{up}}$$

measure experimentally



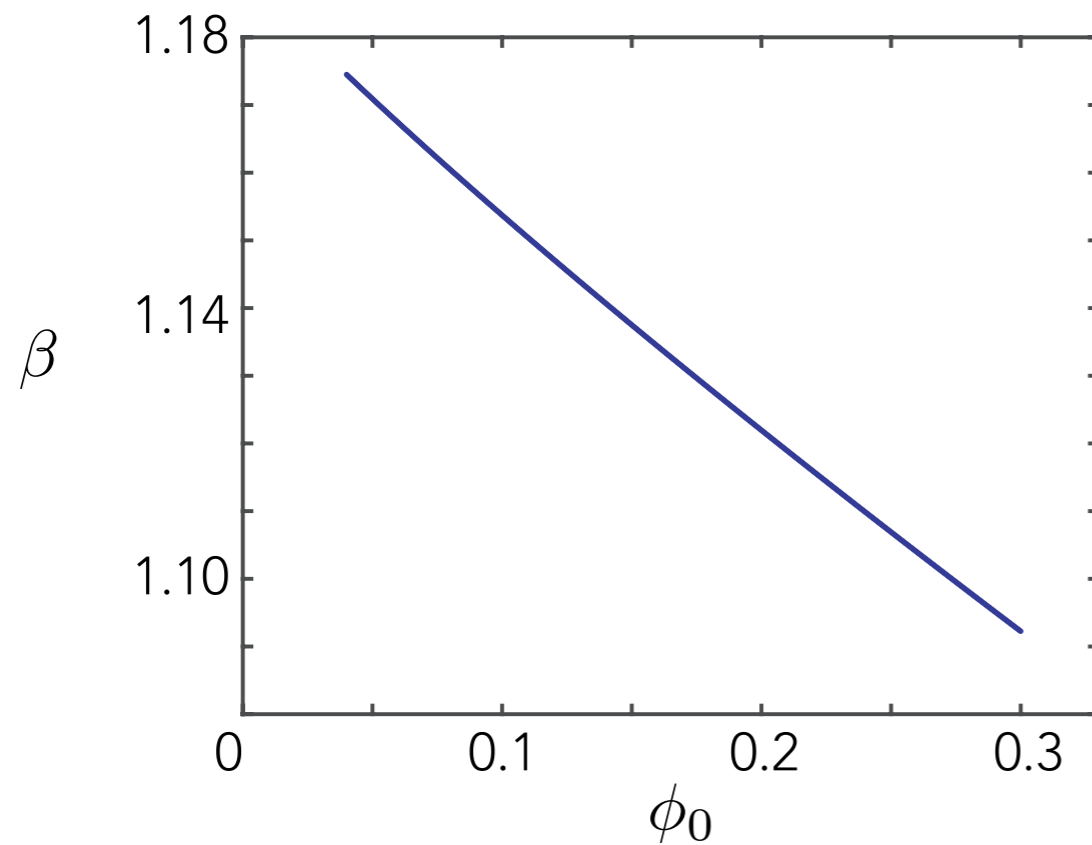
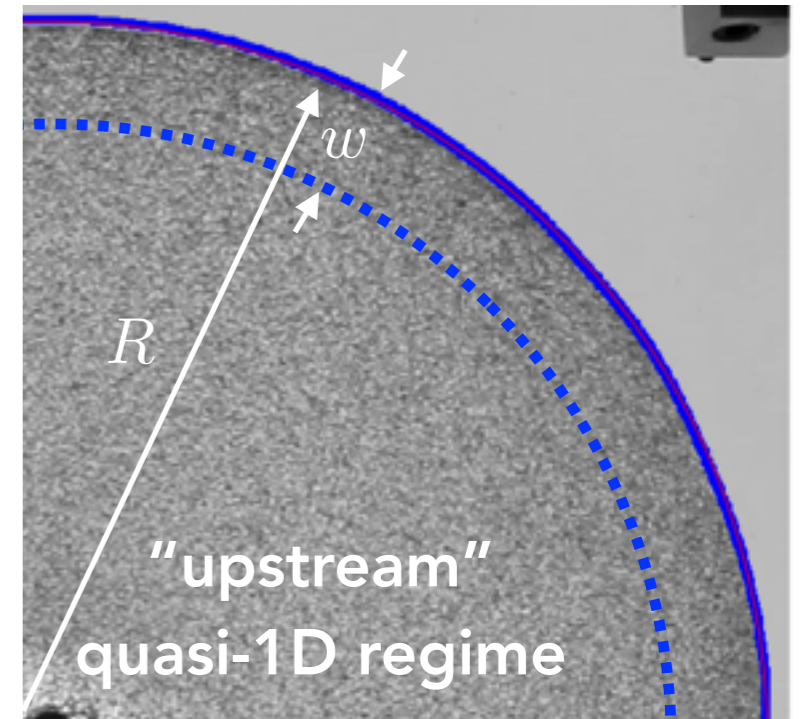
MODEL VALIDATION:

from **accumulation** to **fingering**

mass conservation
in upstream
regime

$$\phi_0 Q = 2\pi r \int_{-h/2}^{h/2} v_r^p(z) \phi(z) dz$$

$$\beta = \phi_0 / \bar{\phi}_{\text{up}}$$



Rate of particle accumulation
decreases with increasing ϕ_0 .



Rate of particle accumulation
does not directly determine
likelihood of fingering.

MODEL VALIDATION:

from **accumulation** to **fingering**

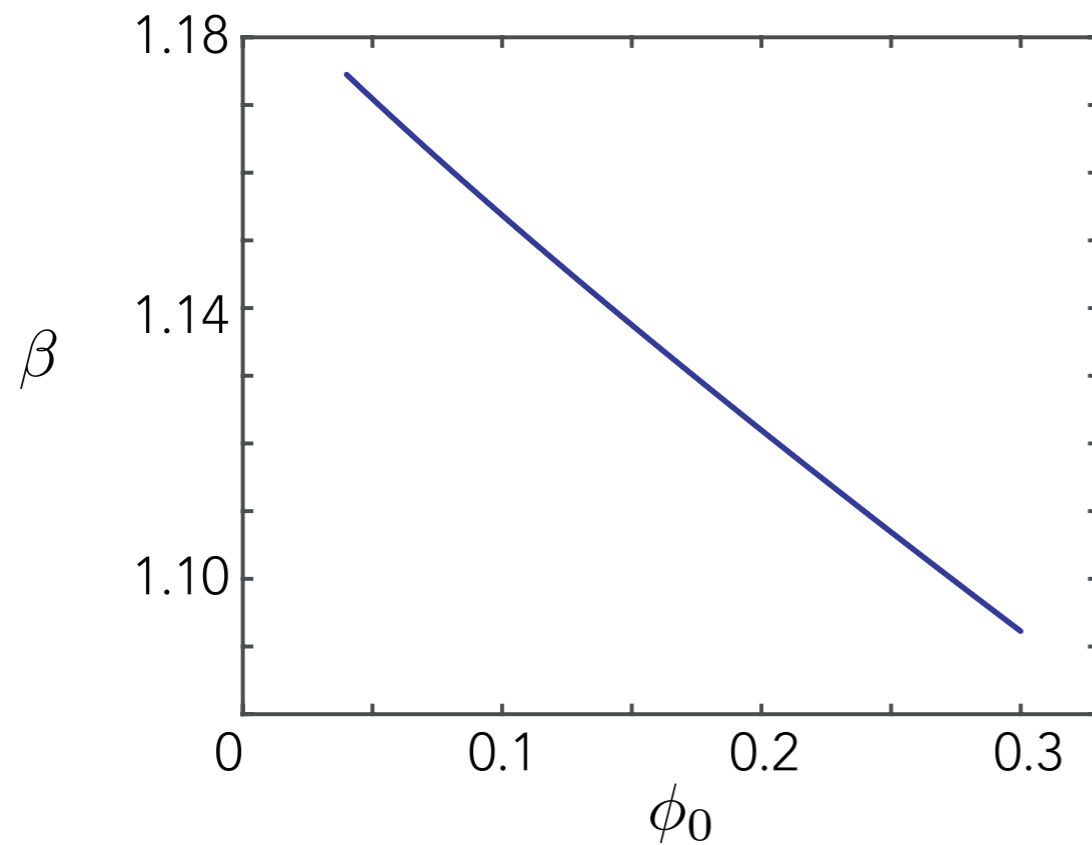
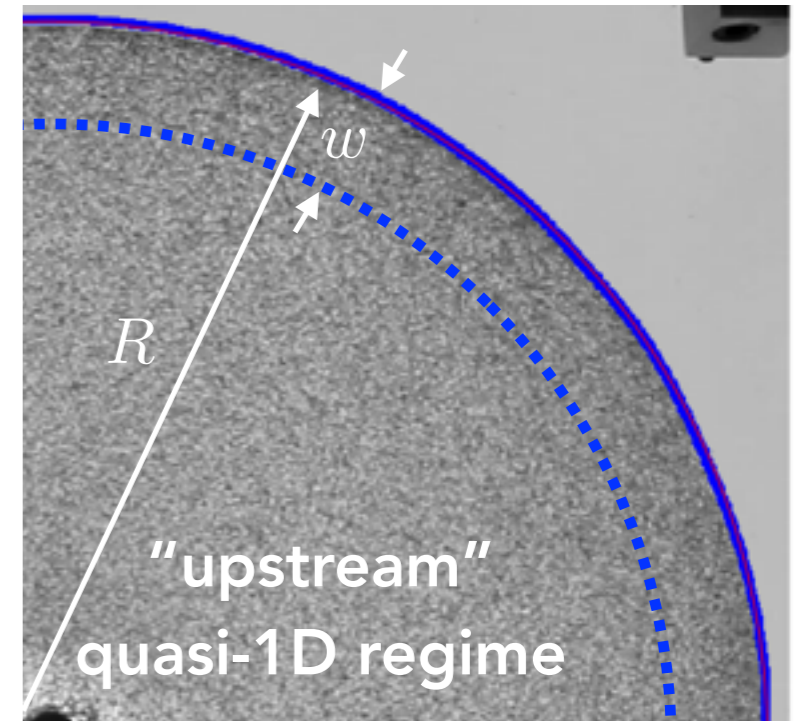
mass conservation
in upstream
regime

$$\phi_0 Q = 2\pi r \int_{-h/2}^{h/2} v_r^p(z) \phi(z) dz$$

$$\beta = \phi_0 / \bar{\phi}_{\text{up}}$$

$$V_{\text{accum}}^{*p} = \frac{V^p - V_{\text{up}}^p}{V^p} \sim \phi_0 \left(1 - \frac{1}{\beta} \right)$$

where $V^p = \phi_0 \pi R^2 h$ & $V_{\text{up}}^p = \frac{\phi_0}{\beta} \pi (R - w)^2 h$



MODEL VALIDATION:

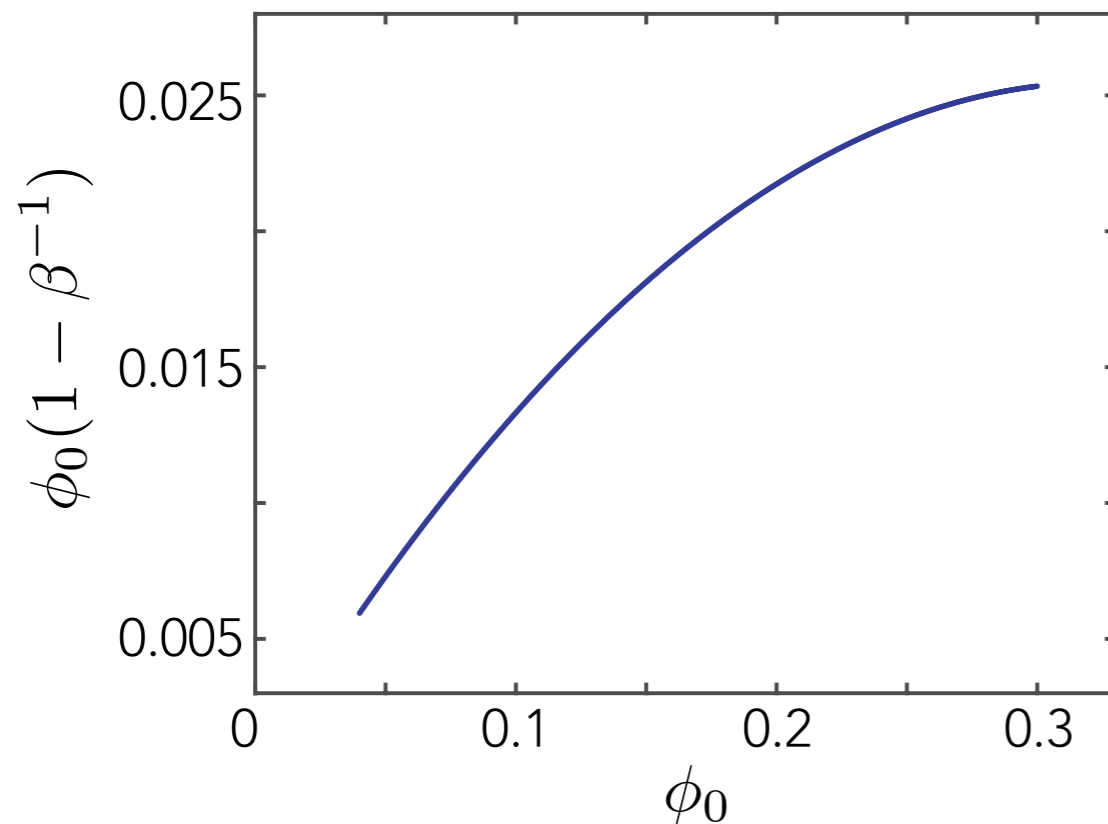
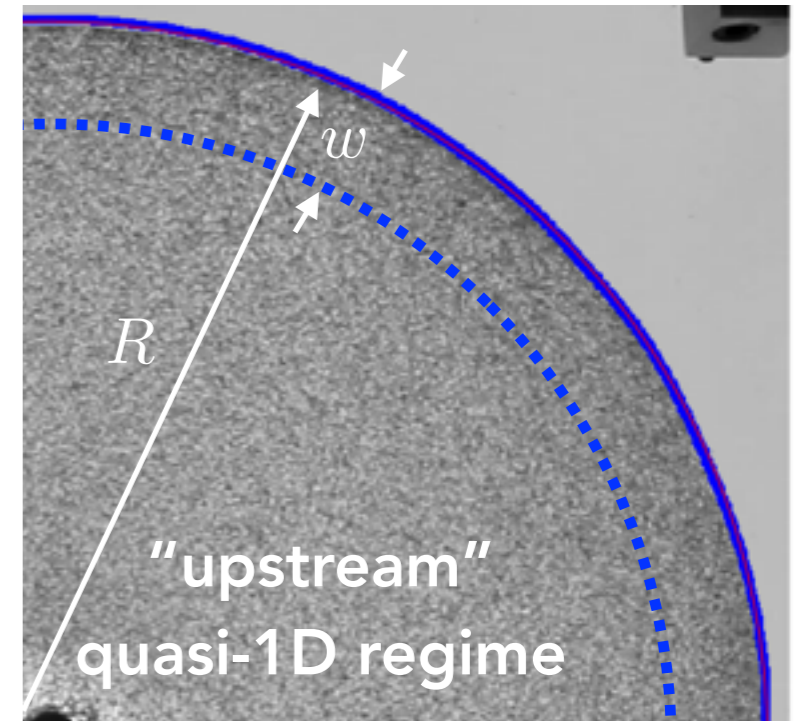
from **accumulation** to **fingering**

mass conservation
in upstream
regime

$$\phi_0 Q = 2\pi r \int_{-h/2}^{h/2} v_r^p(z) \phi(z) dz$$

$$\beta = \phi_0 / \bar{\phi}_{\text{up}}$$

$$V_{\text{accum}}^{*p} = \frac{V^p - V_{\text{up}}^p}{V^p} \sim \phi_0 \left(1 - \frac{1}{\beta}\right)$$



More particles collect near the interface with increasing ϕ_0 .



More likely to finger with increasing ϕ_0 .

Xu, Kim & Lee [in review]

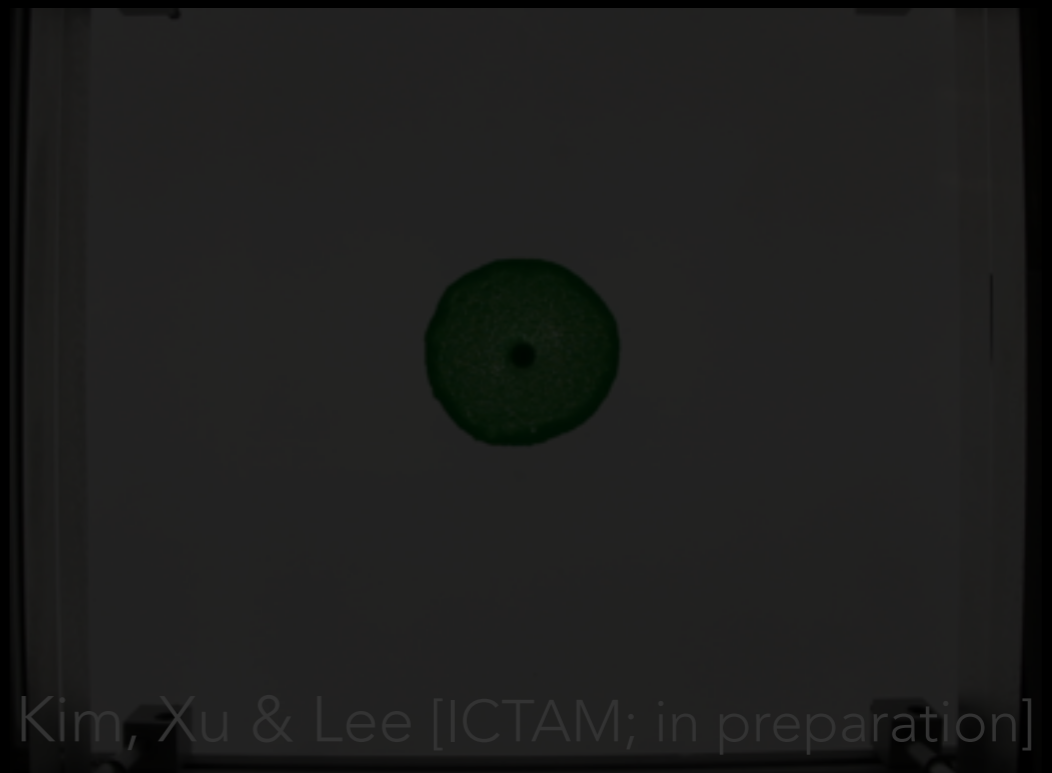
particle-induced fingering

Summary: characterization of particle-induced fingering; continuum model formulation

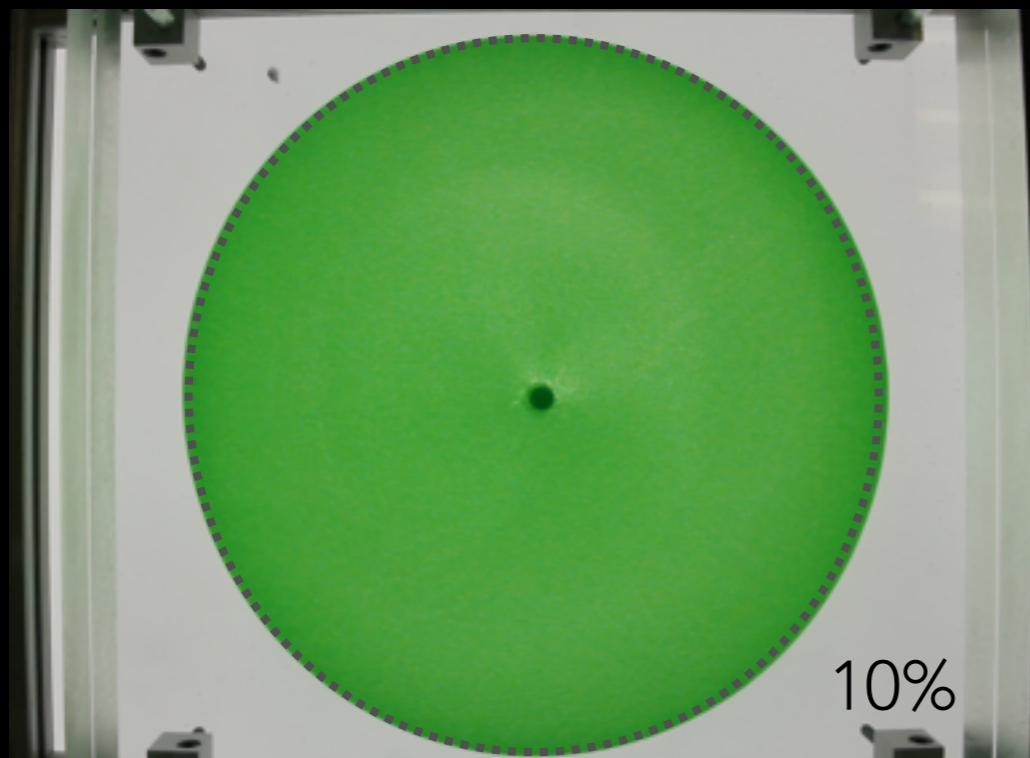
On-going: prediction of the onset of fingering based on stability analysis

Big picture: coupled dynamics of particles & interface dynamics

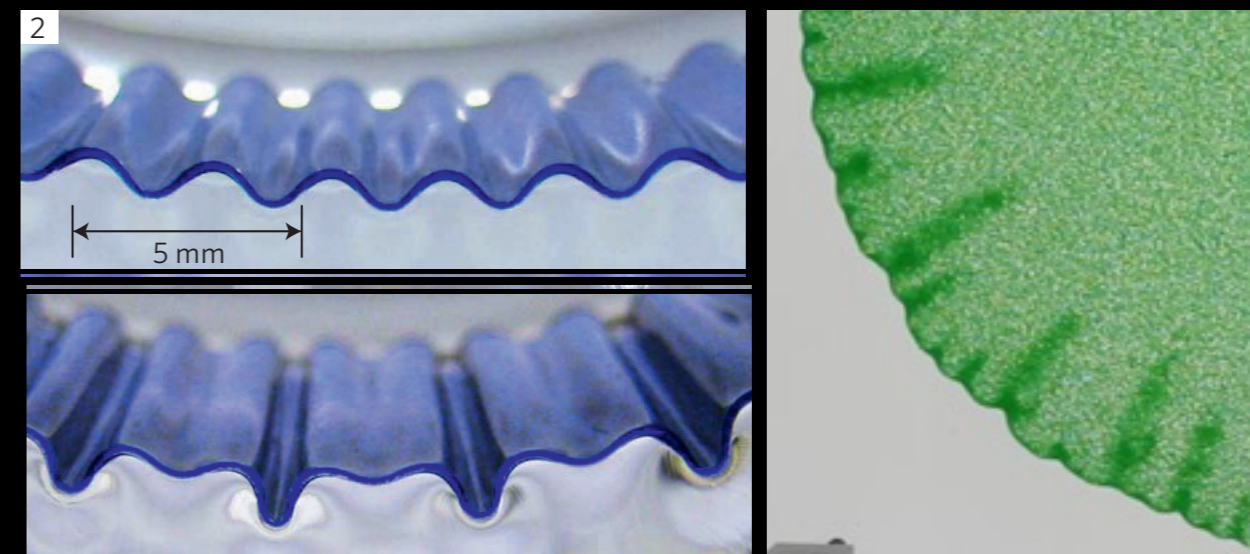
formation & breakage of particle band



effect of particles on **draining**



pattern formation with analogy to elastic instability



Brau et al 2011

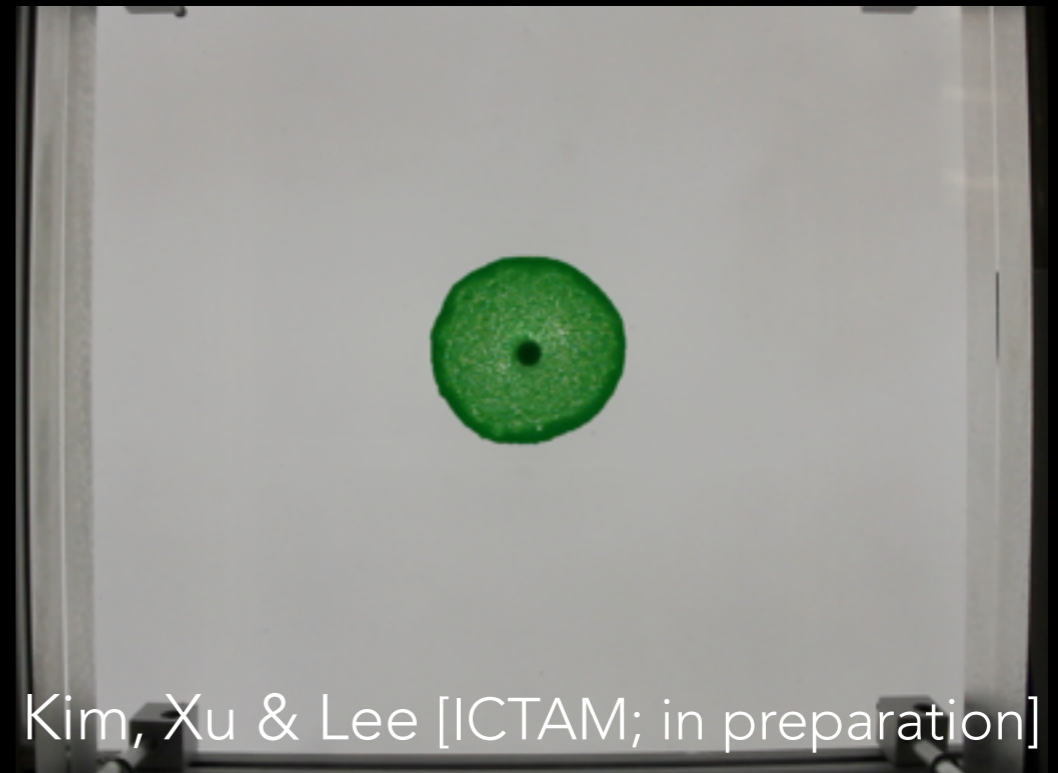
particle-induced fingering

Summary: characterization of particle-induced fingering; continuum model formulation

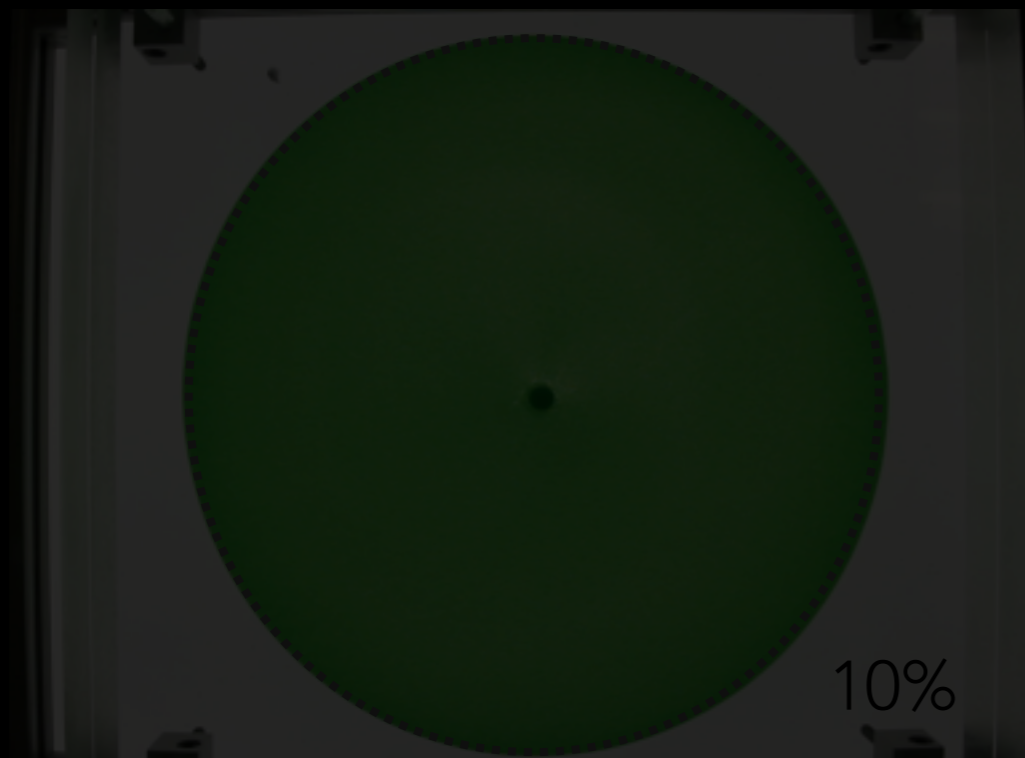
On-going: prediction of the onset of fingering based on stability analysis

Big picture: coupled dynamics of particles & interface dynamics

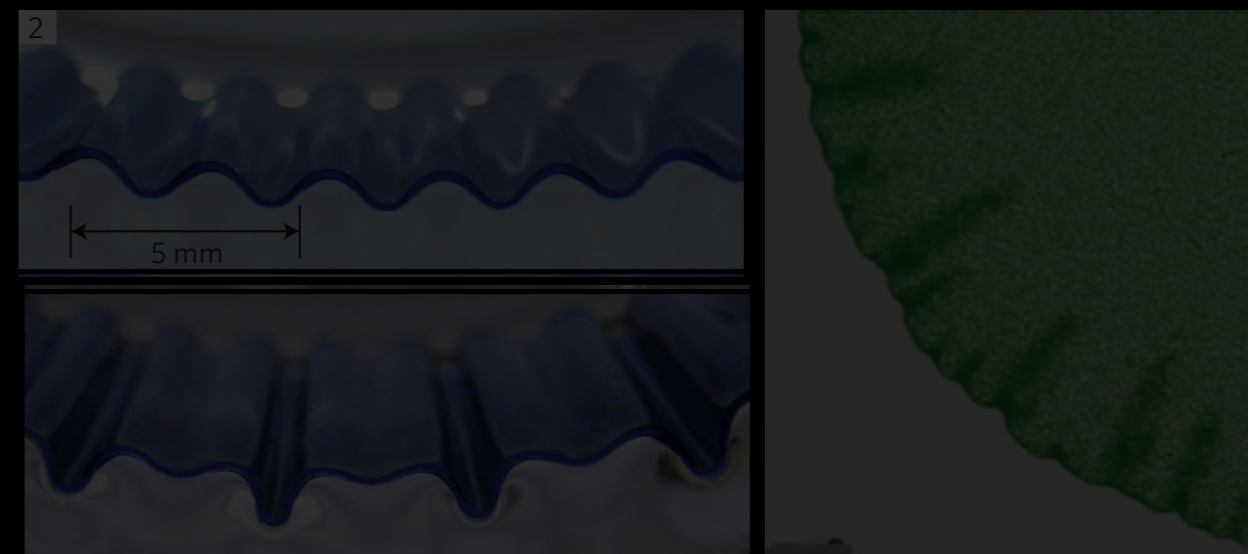
formation & breakage of particle band



effect of particles on **draining**



pattern formation with analogy to elastic instability



Brau et al 2011

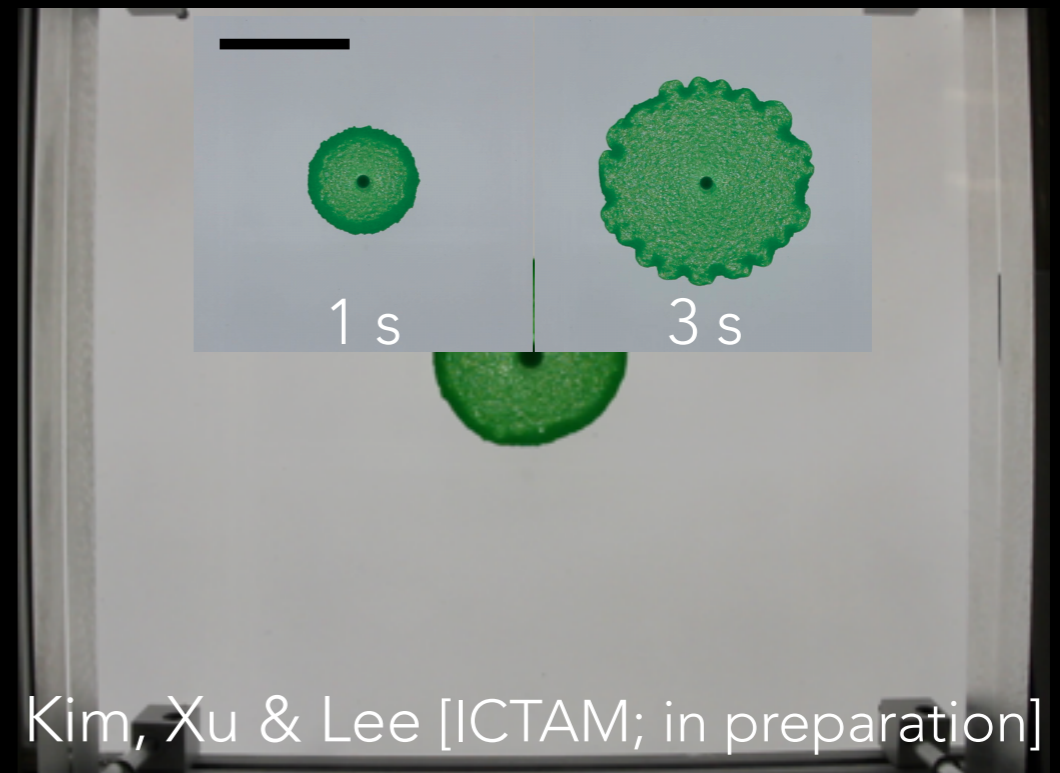
particle-induced fingering

Summary: characterization of particle-induced fingering; continuum model formulation

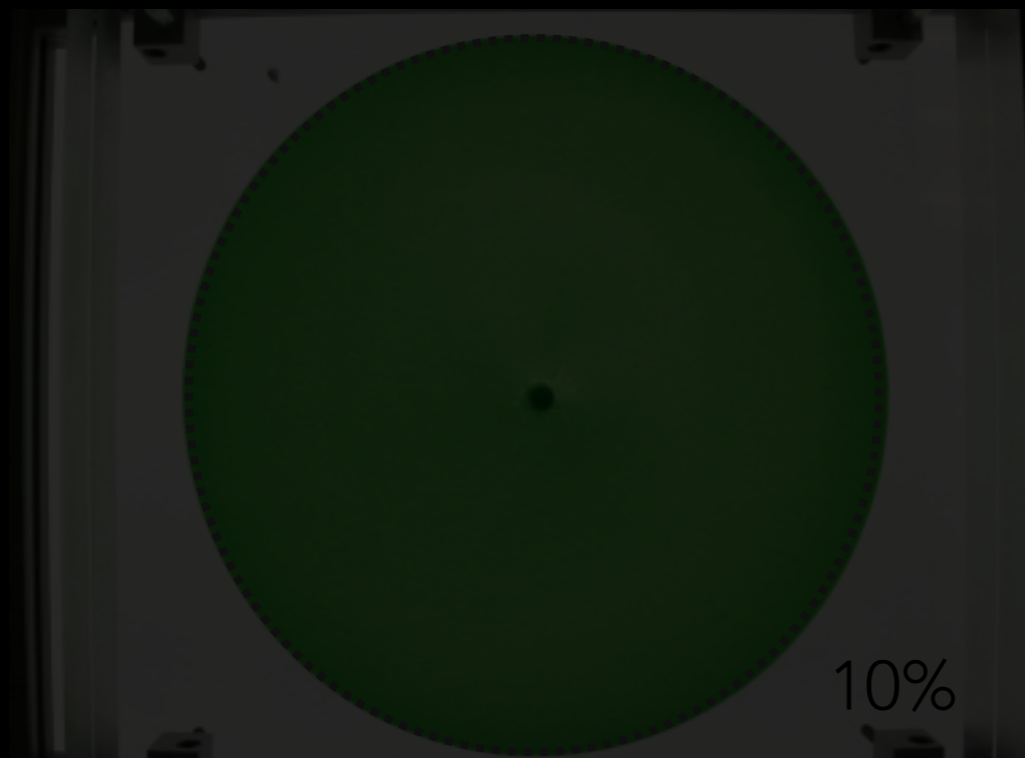
On-going: prediction of the onset of fingering based on stability analysis

Big picture: coupled dynamics of particles & interface dynamics

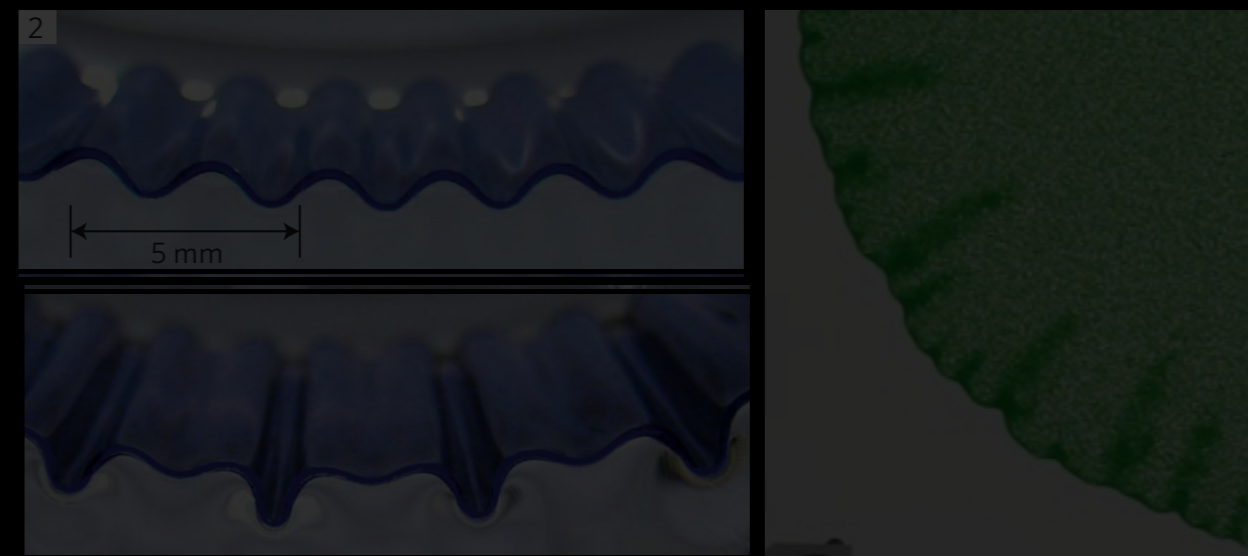
formation & breakage of particle band



effect of particles on **draining**



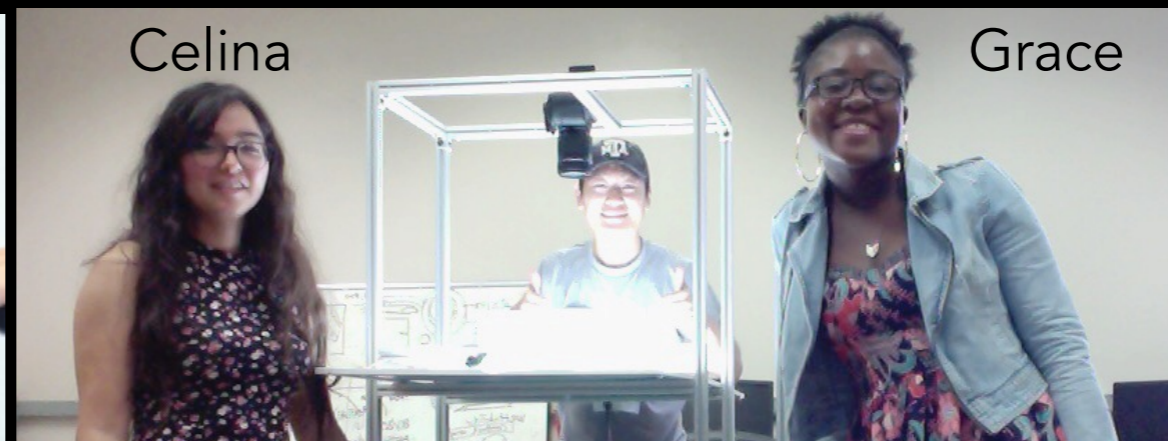
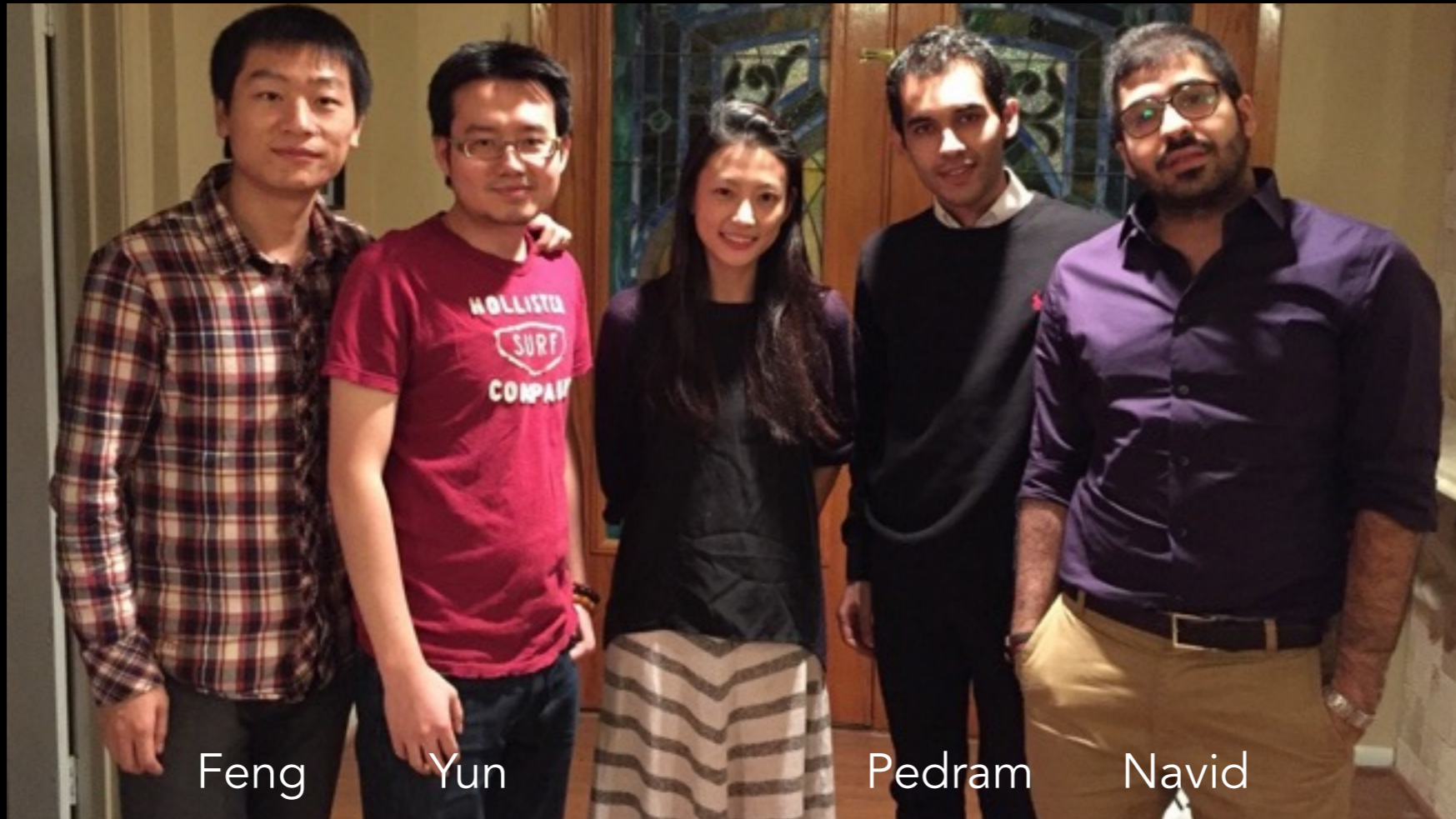
pattern formation with analogy to elastic instability



Brau et al 2011

DrIPs

DROPS, INTERFACES & PARTICULATE SYSTEMS



Thank you.